

Nidec

All for dreams

PRECISION CUTTING TOOLS HANDBOOK

HOBS / GEAR SHAPER CUTTERS / SHAVING CUTTERS
BROACHES / OTHER PRODUCTS



NIDEC MACHINE TOOL CORPORATION

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A Manufacturing System with Three Global Bases to Respond to Global Needs

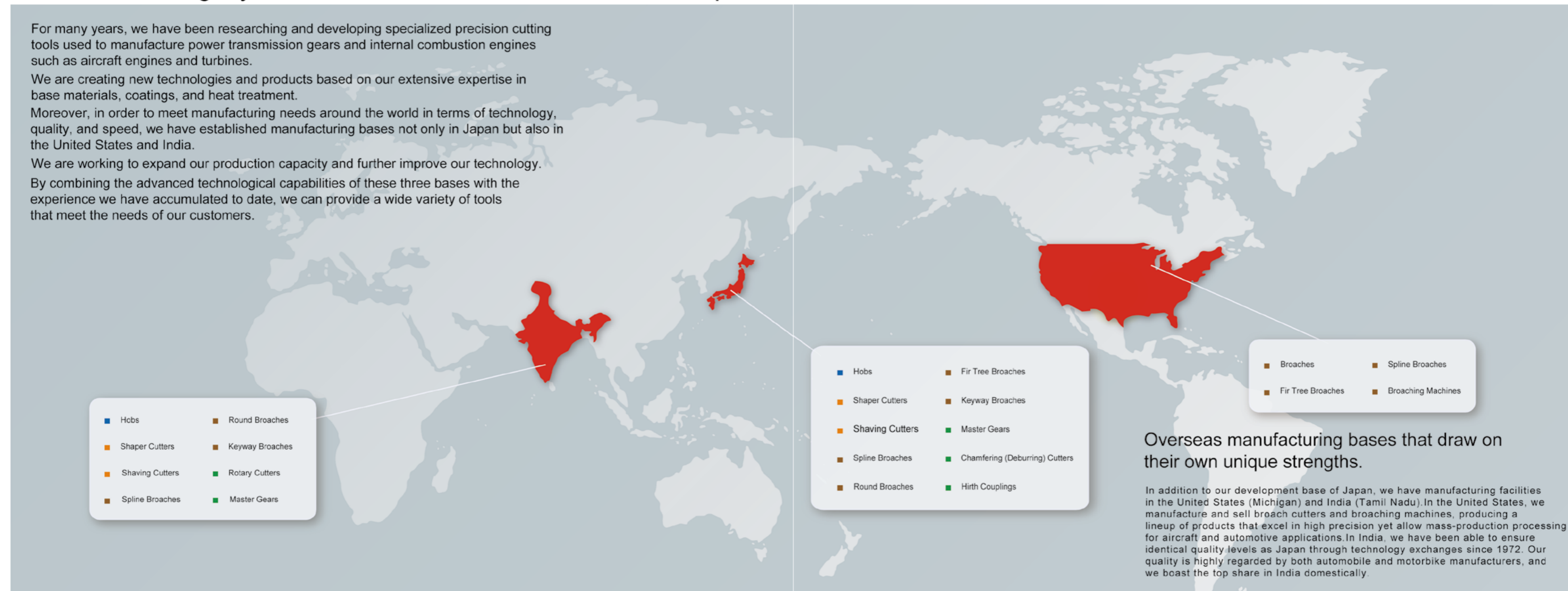
For many years, we have been researching and developing specialized precision cutting tools used to manufacture power transmission gears and internal combustion engines such as aircraft engines and turbines.

We are creating new technologies and products based on our extensive expertise in base materials, coatings, and heat treatment.

Moreover, in order to meet manufacturing needs around the world in terms of technology, quality, and speed, we have established manufacturing bases not only in Japan but also in the United States and India.

We are working to expand our production capacity and further improve our technology.

By combining the advanced technological capabilities of these three bases with the experience we have accumulated to date, we can provide a wide variety of tools that meet the needs of our customers.



Overseas manufacturing bases that draw on their own unique strengths.

In addition to our development base of Japan, we have manufacturing facilities in the United States (Michigan) and India (Tamil Nadu). In the United States, we manufacture and sell broach cutters and broaching machines, producing a lineup of products that excel in high precision yet allow mass-production processing for aircraft and automotive applications. In India, we have been able to ensure identical quality levels as Japan through technology exchanges since 1972. Our quality is highly regarded by both automobile and motorbike manufacturers, and we boast the top share in India domestically.

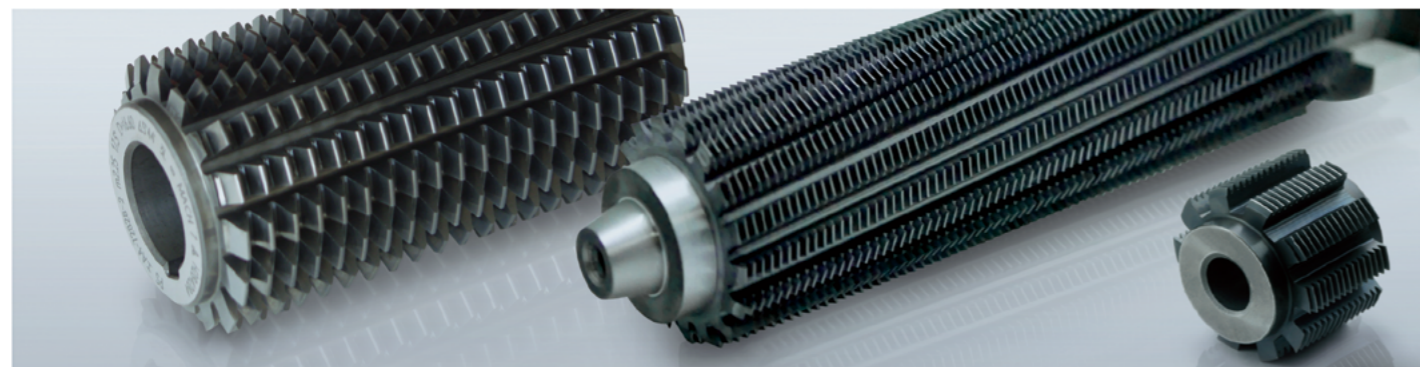
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HOBS

Hobs, with their ability to create gears with superior efficiency, are widely used in automobiles, construction and industrial machinery, as well as for processing power transmission gears for marine vessels and aircraft. We can manufacture tools with the optimum combination of dimensions, such as outer diameter, overall length, bore diameter, and number of gashes, as well as tool materials and coatings. We can also provide

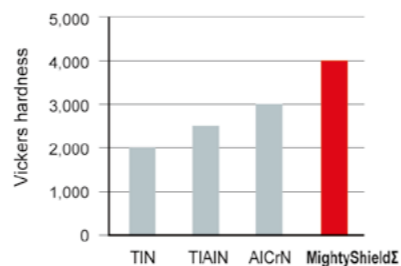
non-involute tooth profiles such as circular arcs, cycloids, and sprocket tooth profiles. In addition, we can manufacture hobs with small-diameter handles and small module hobs. Hobs using Our MightyShield Σ coating on their cutting edges provide all-round performance in any cutting situation, wet or dry, in a wide range of processing areas (HSS hobs, carbide hobs).



MightyShield Σ

Features

- Longer tool life with coating film that offers superior wear resistance (film hardness: Hv 4,000)
- Supports a wide range of processing areas (HSS hobs, carbide hobs).
- Wet or dry, maximum performance whatever the cutting environment.



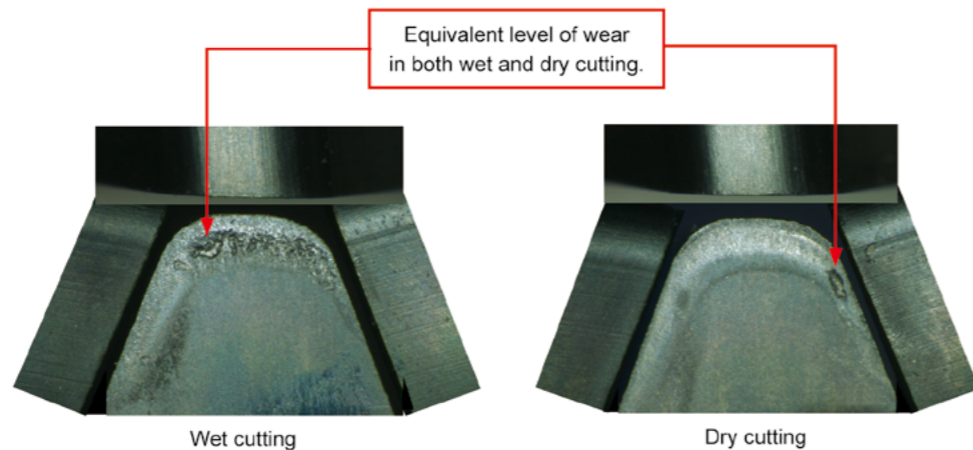
Example

Combined with GRANMET SF, a new material for hobs (cutting speed: 350 m/min)

Combining the new GRANMET SF material with MightyShield Σ allows

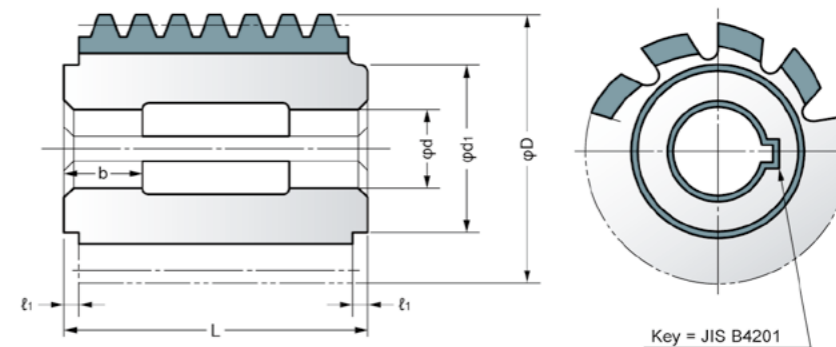
- Cutting speeds in excess of 300 m/min.
- Wet and dry cutting.
(No cracks in the cutting edge during wet cutting)

Workpiece: m 2.7 PA 20° HA 30° NT 69 Material: Carburized steel
Cutter: 4 starts 16 Z Material: GRANMET SF Coating: Mighty Shield Σ
Cutting conditions: Cutting speed: 350 m/min Axial travel: 2.3 mm/rev
Processing No.: 50 (non-shift) Wet (water-lubricated) and dry cutting



Dimensions and Precision Standard

Dimensions



Unit: mm

Module (m)			D	L	d		Reference			
1	2	3			Type A	Type B	N	d ₁	b	ℓ ₁
1			50	50	22	22.225	12	34	12	4
1.25								36	14	
1.5										
2	1.75		60	60	10	26.988	38	15		
2.5	2.25		65	65			42	16		
3	2.75		70	70			45	18		
	3.5	3.25	75	75	27	31.75	9	50	20	
4	4.5	3.75	80	80				55	22	
5	5.5		85	85				24	25	
6		6.5	90	90	32	38.1	8	28	5	
	7		95	95				32	36	
8	9		100	100				40	40	
10	11		110	110	40	50.8	6	44		
12	14		115	115				48	52	
16	18		120	120				58	62	
20	22		125	125	50	80	8	68		
			130	130				75	75	
25			130	160				80	80	

Precision Standard

Unit: μ m

No.	Item	Standard diameter (mm)	Grade	Tolerance											
				Type A	Type B	8	10	13	22	-	27	32	40	50	-
1	Bore diameter	AAA	AA	A	+2.5 (H3)	+3 (H3)	+6 (H4)	+7 (H4)	+8 (H4)	+8 (H4)	+8 (H4)				
					0	0	0	0	0	0	0	0	0	0	
					+4 (H4)	+5 (H4)	+9 (H5)	+11 (H5)	+13 (H5)	+13 (H5)	+13 (H5)	+13 (H5)	+13 (H5)	+13 (H5)	
					0	0	0	0	0	0	0	0	0	0	0

No.	Item	Module	Grade	Margin or tolerance					
				1 or more 2 or less	More than 2 3.5 or less	More than 3.5 6.3 or less	More than 6.3 10 or less	More than 10 16 or less	More than 16 25 or less
2	Boss	Peripheral runout	AAA	2	3	3	4	5	-
			AA	3	3	4	5	6	9
			A	5	5	6	8	10	14
3	Surface deflection	AAA	2	2	2	3	4	-	
		AA	2	3	3	4	5	7	
		A	4	4	5	6	8	11	
4	Outside periphery	Gear cutting edge deflection	AAA	12	13	16	19	25	-
			AA	15	17	20	25	32	45
			A	24	26	32	40	50	71

Unit: μm

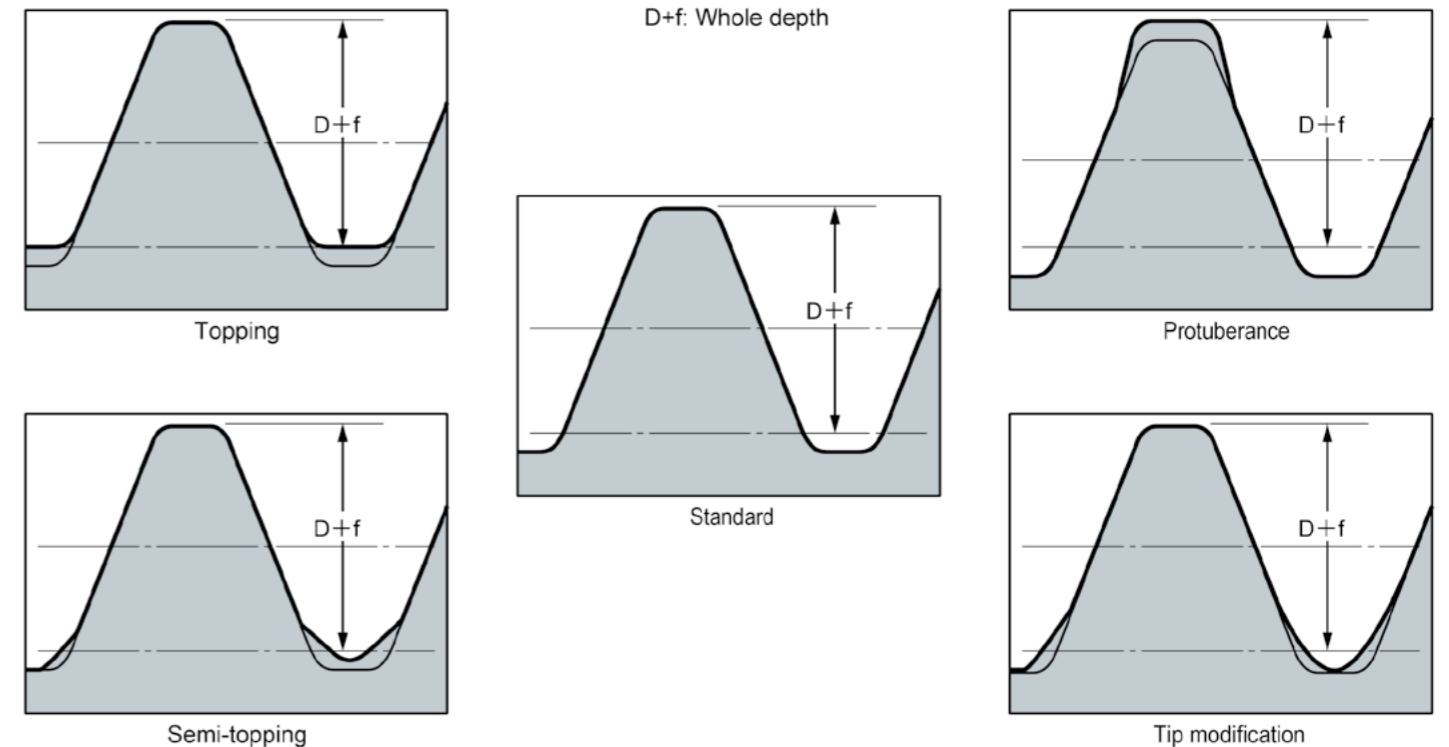
No.	Item	Module		Permissible value or tolerance							
				Grade	Permissible value or tolerance						
					1 or more 2 or less	More than 2 3.5 or less	More than 3.5 6.3 or less	More than 6.3 10 or less	More than 10 16 or less	More than 16 25 or less	
5	Vicinal division error	AAA	12	13	16	19	25	-			
		AA	15	17	20	25	32	45			
		A	24	26	32	40	50	71			
6	Cumulative division error	AAA	22	25	30	38	48	-			
		AA	28	32	36	45	60	85			
		A	45	50	60	70	95	132			
7	Gash	AAA	9	11	12	15	20	-			
		AA	12	13	15	19	25	36			
		A	18	21	25	30	40	56			
8	Lead error	Grade		Tolerance							
				32 mm or less	More than 32 mm						
		AAA	16	50							
AAA	AA	A	20	60							
			25	80							
9	Profile error A	Single start	AAA	4	4	5	6	8	-		
			AA	5	5	6	8	10	14		
			A	8	8	10	12	16	22		
		Threefold start	AAA	5	6	7	8				
			AA	7	7	8	11				
			A	11	12	14	17				
		Fivefold start	AAA	7	8						
			AA	8	10						
			A	13	15						
		10	Tooth thickness error (-)	Single start	AAA	26	30	36	42	56	-
					AA	34	38	42	56	71	100
					A	34	38	42	56	71	100
Threefold start	AAA			38	42	50	60				
	AA			48	53	60	75				
	A			48	53	60	75				
Fivefold start	AAA			48	53						
	AA			60	67						
	A			60	67						
11	Cutter addendum error (+)			Single start	AAA	38	42	50	60	80	-
					AA	48	53	60	75	100	140
					A	48	53	60	75	100	140
		Threefold start	AAA	53	60	67	85				
			AA	67	71	85	106				
			A	67	71	85	106				
Fivefold start	AAA	67	75								
	AA	85	95								
	A	85	95								
12	Vicinal error	Single start	AAA	3	4	4	6	7	-		
			AA	4	5	6	7	9	12		
			A	7	8	9	11	14	20		
		Threefold start	AAA	5	5	6	8				
			AA	6	7	8	10				
			A	10	11	12	15				
		Fivefold start	AAA	6	7						
			AA	8	8						
			A	12	13						
13	1-axial pitch Cumulative error A	Single start	AAA	6	7	8	10	13	-		
			AA	8	8	10	12	16	22		
			A	12	13	16	19	25	36		
		Threefold start	AAA	8	10	11	14				
			AA	11	12	14	17				
			A	17	19	22	28				
Fivefold start	AAA	11	12								
	AA	13	15								
	A	21	24								
14	3-axial pitch Cumulative error	Single start	AAA	11	12	14	17	22	-		
			AA	13	15	17	21	28	40		
			A	21	24	28	34	45	63		
		Threefold start	AAA	14	16	19	24				
			AA	18	20	24	30				
			A	28	32	38	48				
Fivefold start	AAA	19	21								
	AA	24	26								
	A	38	42								

Unit: μm

No.	Item	Module		Tolerance or permissible tolerance					
				Grade	Tolerance or permissible tolerance				
					1 or more 2 or less	More than 2 3.5 or less	More than 3.5 6.3 or less	More than 6.3 10 or less	More than 10 16 or less
15	Line of action vicinal pitch error	Single start	AAA	3	4	4	6	7	-
			AA	4	5	6	7	9	12
			A	7	8	9	11	14	20
		Threefold start	AAA	5	5	6	8		
			AA	6	7	8	10		
			A	10	11	12	15		
		Fivefold start	AAA	6	7				
			AA	8	8				
			A	12	13				
16	Line of action cumulative division error	Single start	AAA	8	8	10	12	16	-
			AA	10	11	12	15	20	28
			A	15	17	19	25	32	45
		Threefold start	AAA	11	12	14	17		
			AA	13	15	17	21		
			A	21	24	28	34		
		Fivefold start	AAA	13	15				
			AA	17	19				
			A	26	30				
17	Single pitch error	Single start	AAA	5	5	6	8	10	-
			AA	6	7	8	10	12	18
			A	10	11	12	15	20	28
		Threefold start	AAA	5	6	7	8		
			AA	7	7	8	11		
			A	11	12	14	17		
Fivefold start	AAA	7	8						
	AA	8	10						
	A	13	15						
18	Vicinal pitch error	Single start	AAA	8	10	11	14	14	-
			AA	11	12	14	17	22	32
			A	17	19	22	28	36	50
		Threefold start	AAA	12	13	15	19		
			AA	15	16	19	24		
			A	24	26	30	38		
		Fivefold start	AAA	15	17				
			AA	19	21				
			A	30	34				
19	3 Axial pitch error	Single start	AAA	8	10	11	14	14	-
			AA	11	12	14	17	22	32
			A	17	19	22	28	36	50
		Threefold start	AAA	12	13	15	19		
			AA	15	16	19	24		
			A	24	26	30	38		
Fivefold start	AAA	15	17						
	AA	19	21						
	A	30	34						

Remarks: These precision standards are extracted from JIS B4355-1998.

Profile



Hobs

Shaper Cutters

Shaving Cutters

Broaches

Other Products

Materials and Coatings for Tools

Estimates / Design Specifications

Hobs

Shaper Cutters

Shaving Cutters

Broaches

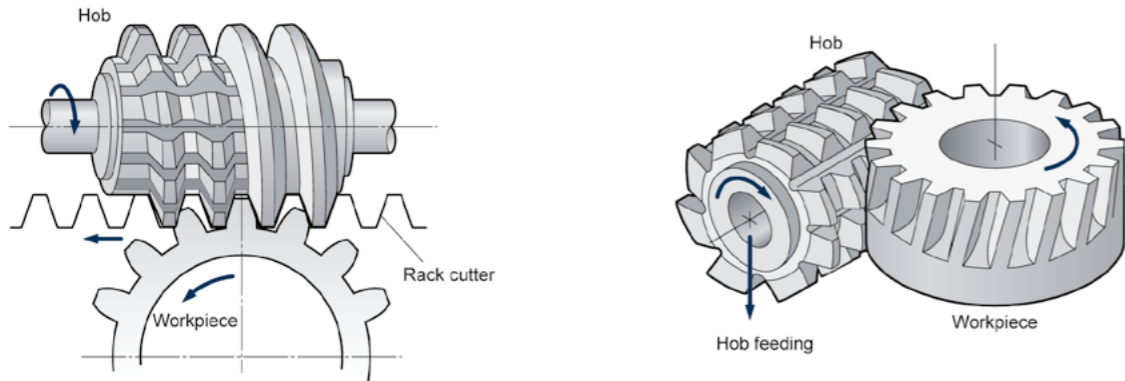
Other Products

Materials and Coatings for Tools

Estimates / Design Specifications

Cutting by Hobbing

Achieve highly efficient and accurate gear cutting—just mount a hob on the hobbing machine, position the hob and the workpiece like a rack and pinion, rotate them in sync, and feed the hob along the workpiece in the direction of the gear tooth width.



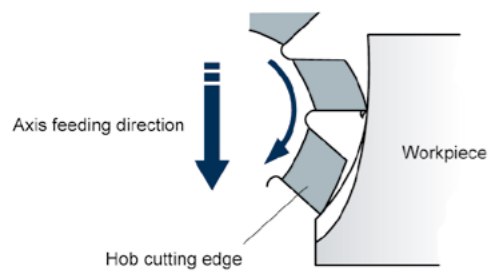
A hob can be seen either as multiple teeth or as a single tooth. One tooth of a workpiece is generated per rotation.

The hob is fed to a workpiece in the gear width direction. Processing efficiency may improve if the number of starts for the hob is increased, but the number of cutting teeth will decrease and cause an increase in the polygonal error. The machine must have sufficient rigidity and strength.

Gear Cutting Methods in Hobbing

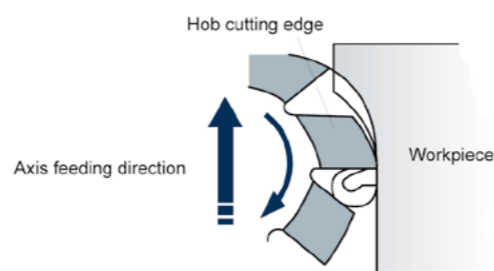
Conventional hobbing

The hob rotates from the top to the bottom face of a workpiece.



Climb hobbing

The hob rotates from the bottom to the top face of a workpiece.



Precautions for Sharpening

The cutting surfaces wear, so need to be ground off. This is called sharpening. If sharpening is not carried out properly, the hob will become less precise, and the following issues will occur.

$\Delta\gamma_s$ =Hobbing lateral face lip clearance ($\tan\Delta\gamma_s = \tan\epsilon \cdot \tan\alpha_n \cdot \cos\gamma$)
 ϵ =external lip clearance, α_n =tooth pressure angle, γ =hobbing feeding angle, r_p =hobbing pitch circle diameter

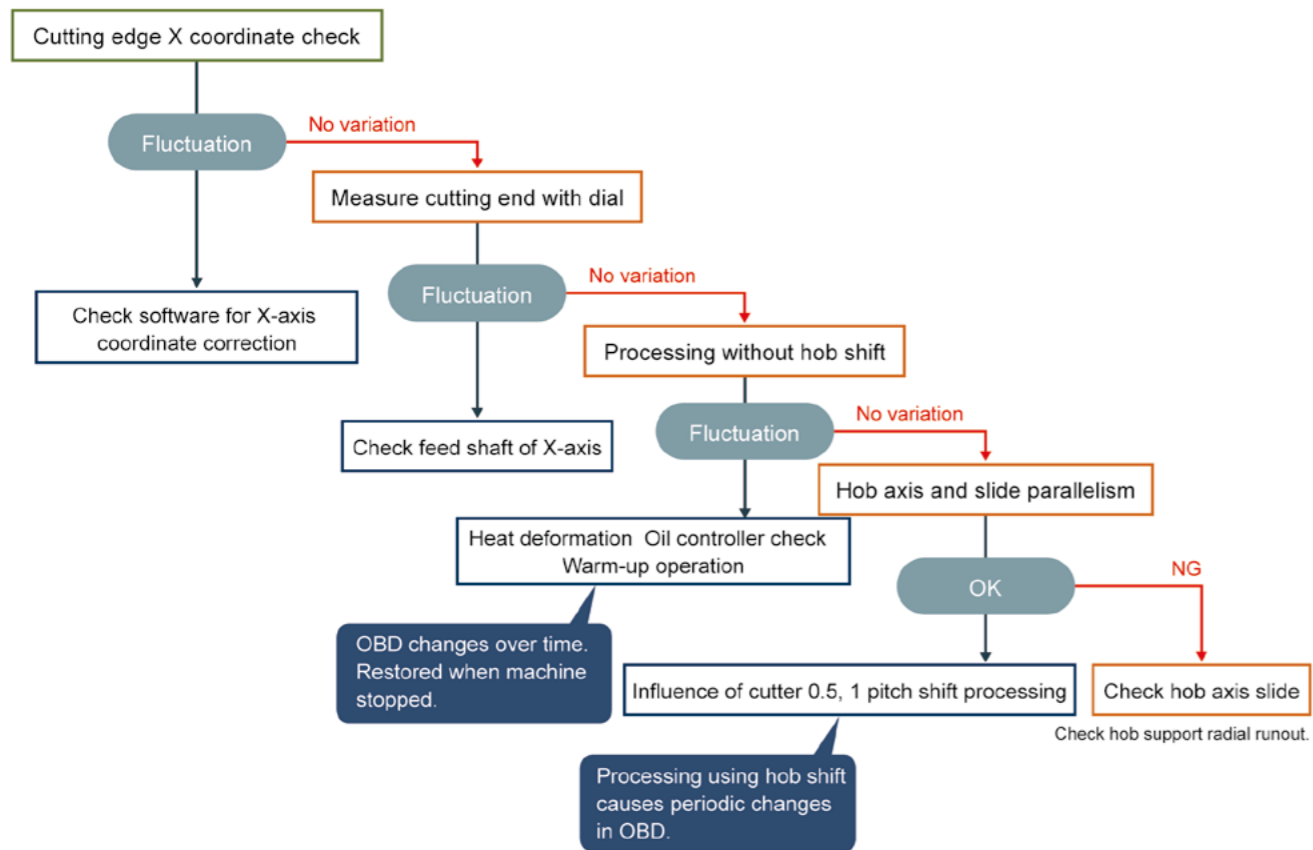
Flute spacing error caused by sharpening	Flute spacing angle error $\Delta\theta$ rad (spacing error)	Helix angle error $\Delta\beta$ rad (lead error)	Cutting face radial direction error δ deg (cutting face angle error)	Cutting face becomes uneven (radial alignment)
Effect on hob and formula for calculating this / Error in normal hobs	<ul style="list-style-type: none"> Uneven pitch in cutting teeth (tooth profile deviation in machined gears) $\Delta t\theta = r_p \cdot \Delta\theta \cdot \tan\Delta\gamma_s$ Pitch error of approx. 6 μm for every 0.1 mm 	<ul style="list-style-type: none"> Expansion and contraction of entire cutting edge pitch (workpiece gear pressure angle deviation) $\Delta t\beta = t_a \cdot \Delta\beta \cdot \tan\Delta\gamma_s$ For every $\Delta\beta = 1^\circ$ expands/contracts at a rate of $\Delta t\beta = 0.001 t_a$ (t_a=axial pitch) 	<ul style="list-style-type: none"> Pressure angle error (workpiece gear pressure angle deviation) $\sin\Delta\alpha = \tan\delta \cdot \cos^2\alpha \cdot \tan\Delta\gamma_s$ For every $\delta = 3^\circ$, error of $\Delta\alpha = 10'$ 	<ul style="list-style-type: none"> Tooth profile error (tooth profile deviation in machined gears) $\Delta t_q = \frac{r_p}{R} \Delta\gamma_s \cdot \tan\Delta\gamma_s$ For every $\Delta\gamma_s = 0.1$ mm, tooth profile error or 6 μm

Hobbing Problems and Causes

Problem	Symptom	Cause
Large undulations	Tooth profile with large undulations	1. Hub runout
		2. Poor lead precision
		3. Poor cutting face pitch
		4. Excessive bore diameter
		5. Poor profile
		6. Inaccurate installation of the hob to the hob arbor
Large collapse	Collapsed tooth form	1. Hub runout
		2. Poor hob profile
	Insufficient meshing length	3. Poor radial alignment
		4. Runout of workpiece during workpiece measurement
Pitch	Poor workpiece pitch	1. Insufficient profile depth
		2. Excessive cutter tip point radius
		3. Poor cutter protuberance profile
		4. Cutter design error
		5. Runout of workpiece during workpiece measurement
Lead	Poor workpiece lead	1. Hub runout
		2. Poor hobbing machine precision
		3. Runout of workpiece during workpiece measurement
Chamfering	Excessive or insufficient chamfering	1. Poor hob chamfering height
		2. Poor workpiece outer diameter size
		3. Cutting run-in size error
	Difference in chamfering amount on each side	4. Poor hob radial alignment
		5. Cutter design error
		6. Hob mounting angle error
External diameter Tooth thickness Root diameter	Workpiece external diameter, tooth thickness, or root diameter defect (Topping profile hob)	1. Poor hob tooth thickness or depth dimensions
		2. Cutting run-in size error
		3. Poor hob radial alignment
		4. Cutter design error
		5. Hob mounting angle error
Tear	Tear in tooth face or periphery	1. Hub runout
		2. Poor lead precision
Fractures	Started from crack	1. Grinding cracks during sharpening
		2. Grinding cracks during tooth profile grinding
	Major fractures	3. Cracking near cutting edge crater due to cutting heat
		4. Cracking in heat treatment process during fabrication
		5. Hob base material defect, excessive hardness, brittleness
Abnormal wear	Coating film stripping	1. Hob base material defect, excessive hardness, brittleness
		2. Run-in during rapid feeding
	Uneven crater wear	3. Workpiece rotates during machining due to loose workpiece clamp
		4. Chips stuck in gashes due to insufficient or inappropriate direction cutting fluid discharge
	Uniform wear	5. Cutting hard materials such as jigs
		6. Poor PVD processing
Wear in the joint tip radius connection	Wear from chips clogging in gashes	• Poor preprocessing
		• Treatment process abnormality
Wear from chips clogging in gashes	Wear from chips clogging in gashes	• Other
		1. Uneven hob shift
Wear from chips clogging in gashes	Wear from chips clogging in gashes	1. Hardness of base material
		2. Poor material
Wear from chips clogging in gashes	Wear from chips clogging in gashes	3. Poor heat treatment
		1. Angularity in the joint tip radius connection
Wear from chips clogging in gashes	Wear from chips clogging in gashes	1. Narrow width of gash
		2. Chips stuck in gashes due to insufficient or inappropriate direction cutting fluid discharge

Standard Size Variation: Troubleshooting

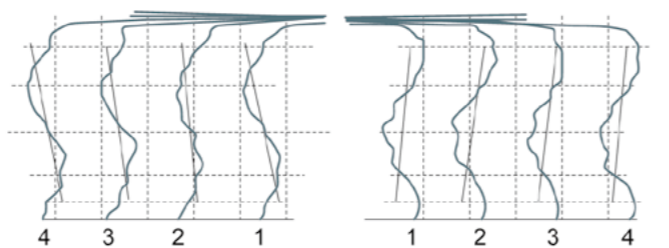
If the OBD suddenly changes or fluctuates, check for the effects of swarf clogging, workpiece rotation, or tears.



Effects of Cutting Load Fluctuations

■ Cause

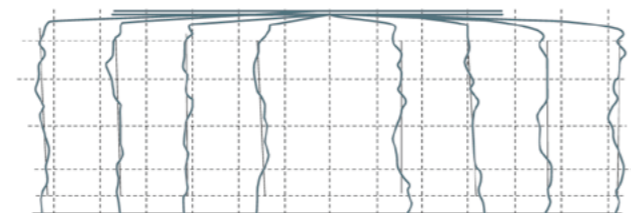
- Cutting force changes from 0 to Max to 0, deflection also changes.
- In particular, load fluctuation at the end of the cut affects machining accuracy.
- In addition, machine rigidity and clearance, mounting rigidity and holding rigidity, and the rigidity of the workpiece itself also have effects.



Distortion of tooth profile due to cutting load fluctuations

■ Verification Method

- if machining accuracy is poor, start with double cutting.
 - If it cleans up, the cause is flexing under load.
 - If it does not, the cause is machine precision.



Tooth profile improvement after double cutting

Hob Setting Angle Error and Tooth Thickness

■ Cause

A hob setting angle error may cause the tooth profile to remain unchanged or the tooth thickness to decrease. The method for discovering the amount of change is shown below.

■ Measures

Finding the amount of change

- Reduction in tooth thickness ΔW (for spur gears)

$$\Delta W = m_n \times \{ \sin^2 \gamma \times \Delta \epsilon^2 / (2 \tan \alpha_n) \} \times (g / \sin^3 \gamma + Z)$$

- m_n : Hob normal module
- α_n : Hob pressure angle
- Z : Number of workpiece teeth
- γ : Hob feed angle
- $\Delta \epsilon$: Hob mounting angle error
- g : Number of starts

- Helical gears

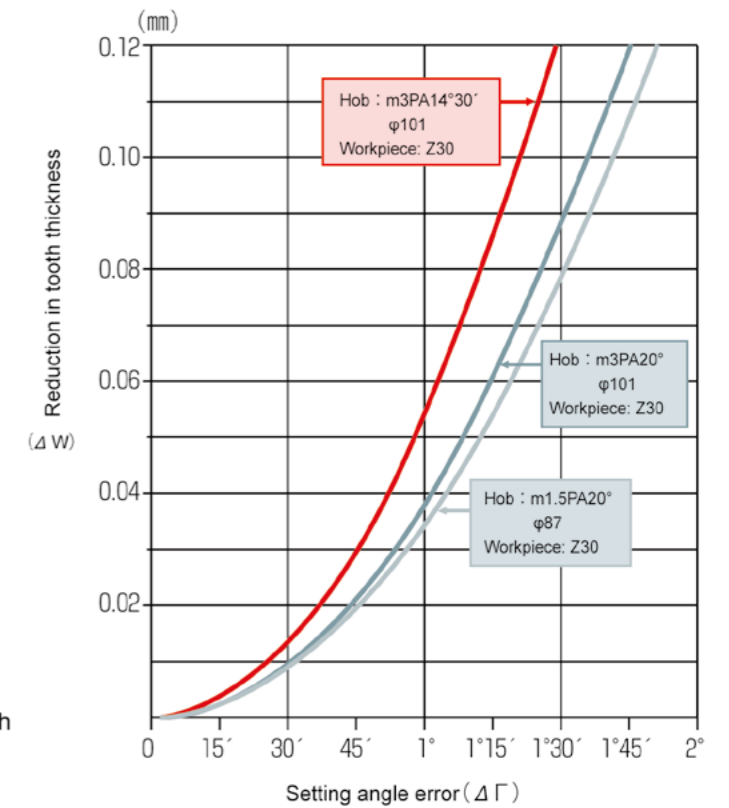
Use the virtual number of teeth Z' instead of Z .

$$Z' = Z / \cos^3 \beta \quad Z : \text{Number of helical gear teeth} \quad \beta : \text{Gear helix angle}$$

- Chamfering hob

Chamfering amount decreases

$$\text{Decrease in chamfer amount } \Delta C = \Delta W / 2 \tan \alpha_n$$



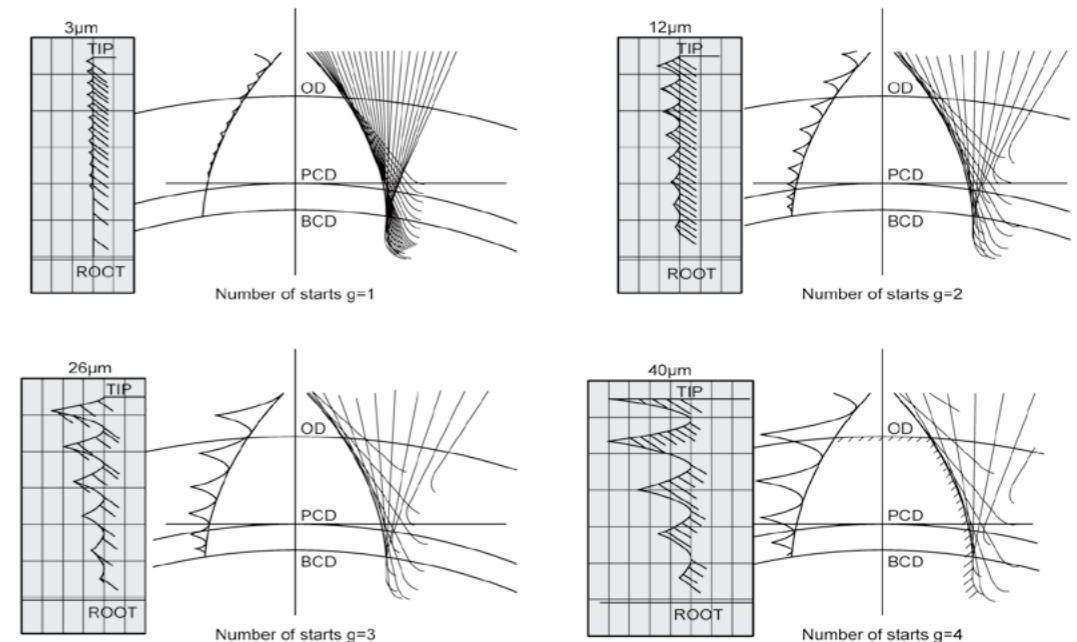
Number of Starts and Polygonal Error

- How to find the polygonal error on the pitch circle

$$\Delta S = \frac{\pi^2 \times s \times \sin \alpha_0 \times g^2 \times m_n}{4 \times I^2 \times Z}$$

- g : Number of starts
- I : Number of gashes
- Z : Number of workpiece teeth

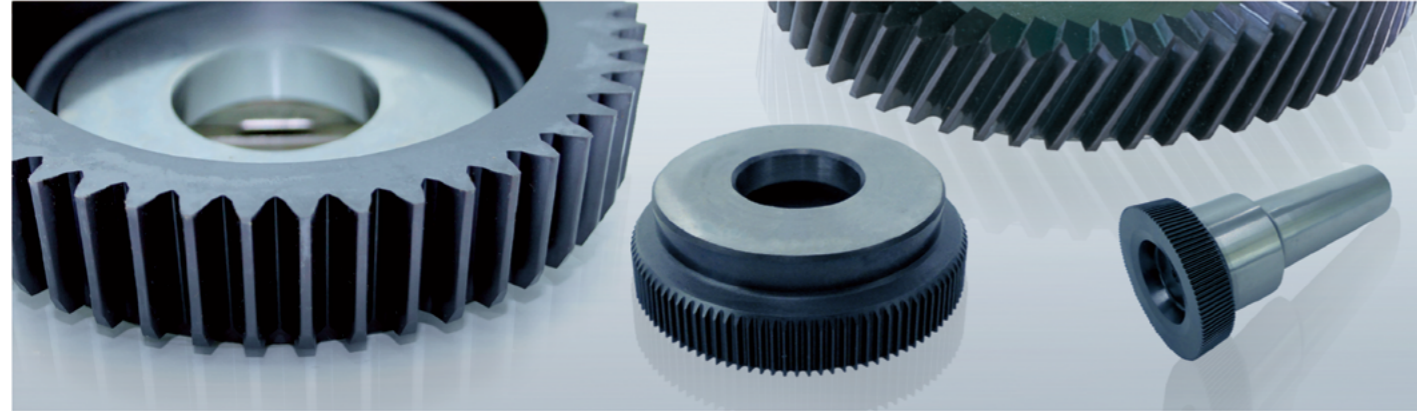
EXAMPLE $\alpha_0=25^\circ$ $m_n=4.5$ $I=12$ $Z=13$ $g=4$ $\Delta S=0.040 m_n$



SHAPER CUTTERS

Shaper cutters are used to process tools for cutting teeth in shapes that hobs cannot handle easily. They are manufactured with our unique 7-axis NC profile grinding machines for involute and non-involute profiles such as circular arcs, cycloids, and sprocket tooth profiles. We offer a lineup of high-quality, high-precision cutters that ensure smooth,

high-precision tooth forms from tip to base, as well as provide long effective tooth lengths. Cutters with the SuperDry series we developed can be used for both wet and dry cutting, offering high efficiency and long life. Moreover, combining these with SS treatment also improves processing quality.

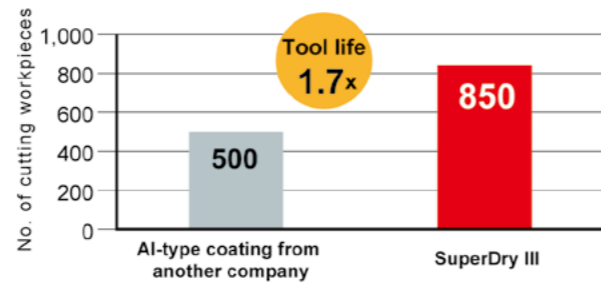


SuperDry III

Features

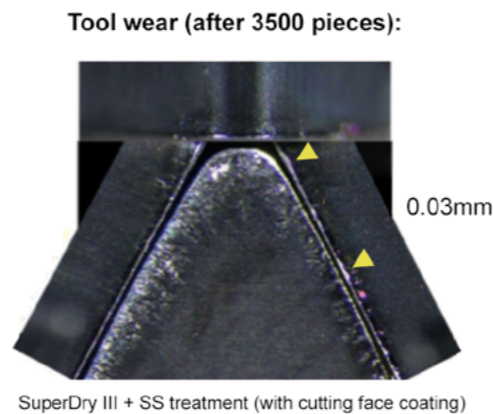
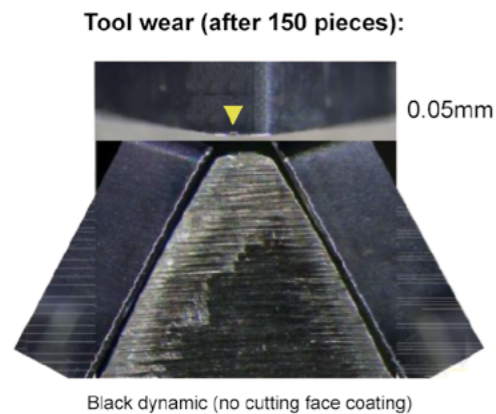
- Harder at high temperatures, improved wear resistance.
- Improved film structure for better adhesiveness.
- Can be used on materials that are hard to cut.
- Increases efficiency and productivity through high-speed processing.

Workpiece: m4 SPUR NT40 (inner teeth) ODφ170 Material: FCD
 Cutter: NT26 ODφ113 Material: MX-1 Coating: SD III (with rake face coating)
 Cutting conditions: No. of strokes: 290/430/430 str/min
 Circumferential feed: 3.0/1.5/1.0 mm/str
 Radial feed: 0.01/0.01/0.01 mm/str



Examples

Workpiece: m2 PA30° SPUR NT27 ODφ52 Material: SCM420
 Cutter: NT62 ODφ127 Material: MAC B Coating: SD III (SS-processed)
 Cutting conditions: No. of strokes: 1100/1100/800 str/min Circumferential feed: 1.5/1.5/0.5mm/str



About SS Treatment

SS treatment is the special treatment of surface finish on cutters.

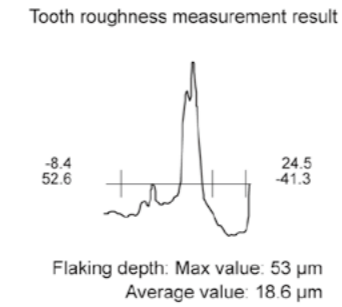
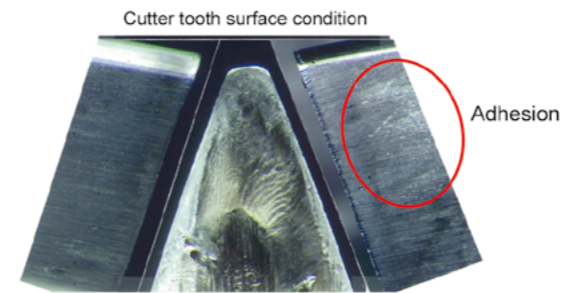
Features

- Deals with flaking and adhesion on workpiece tooth surfaces.
- Deals with adhesion on tool tooth surfaces.
- Special treatment to minimize the roughness of cutter tooth surfaces.

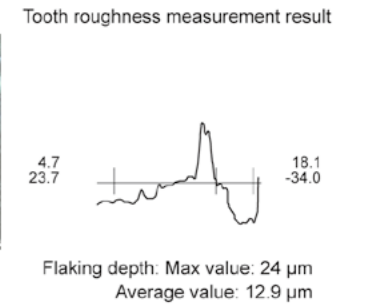
Examples

Workpiece: m2 PA20° HA35°LH NT29 ODφ79 Tooth width 25 Material: SCM420H
 Cutter: ODφ160 φ160 Material: MAC B Black dynamic (no rake face coating)

Processing result by cutter without SS treatment

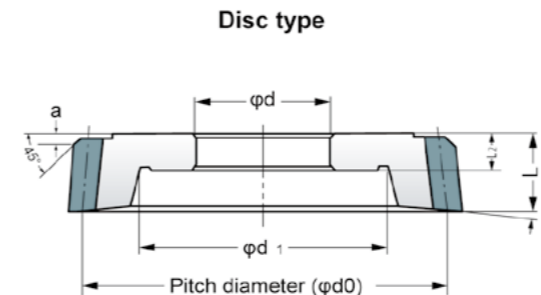


Processing result by cutter with SS treatment



Dimensions and Precision Standard

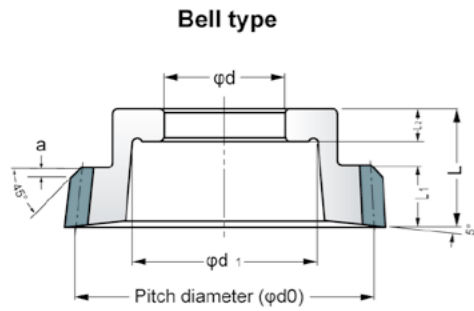
■ Dimensions



Unit: mm

Nominal size	Module (m)	Pitch diameter (d0) (approx.)	d	L	L ₂	d ₁ *	a*
75	0.75 to 1	75	31.742	16	8	50	3
	1.25 to 2	75	31.742	18	8	50	3
	2.25 to 3.5	75	31.742	20	8	50	3
	3.75 to 5	75	31.742	22	10	50	3
100	1	100	31.742	18	10	65	4.5
	1.25 to 2	100	31.742	20	10	65	4.5
	2.25 to 3.5	100	44.450	24	10	65	4.5
	3.75 to 6	100	44.450	26	12	65	4.5
125	6.5 to 7	105	44.450	28	12	65	4.5
	1.5 to 2	125	44.450	22	10	85	4.5
	2.25 to 3.5	125	44.450	24	10	85	4.5
	3.75 to 6	125	44.450	26	12	85	4.5
150	6.5 to 8	135	44.450	30	12	85	4.5
	1.75 to 2	150	44.450	24	12	95	4.5
	2.25 to 3.5	150	44.450	26	12	95	4.5
	3.75 to 6	150	44.450	28	14	95	4.5
175	6.5 to 10	150	44.450	32	14	95	4.5
	2	175	44.450	26	14	110	4.5
	2.25 to 3.5	175	44.450	28	14	110	4.5
	3.75 to 6	175	44.450	30	14	110	4.5
175	6.5 to 10	175	44.450	34	14	110	4.5
	11 to 12	175	44.450	36	16	110	4.5

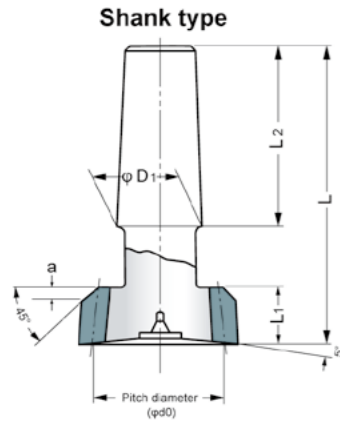
• Tolerance between L and L₂ is per JIS B 0405 Coarse Class
 • Items with an asterisk can be customized as needed.



Unit: mm

Nominal size	Module (m)	Pitch diameter (d0) (approx.)	φd	L	L ₁	L ₂	d ₁ *	a*
50	0.75 to 1	50	19.050	30	12	8	28	3
	1.25 to 2	50	19.050	32	14	8	28	3
	2.25 to 3.5	50	19.050	34	16	8	28	3
	3.75 to 4	60	19.050	38	18	8	28	3
75	0.75 to 1	75	31.742	34	16	8	50	3
	1.25 to 2	75	31.742	36	18	8	50	3
	2.25 to 3.5	75	31.742	38	20	8	50	3
	3.75 to 5	80	31.742	42	22	10	50	3
100	1	100	31.742	38	18	10	65	4.5
	1.25 to 2	100	31.742	40	20	10	65	4.5
	2.25 to 3.5	100	or	42	22	10	65	4.5
	3.75 to 6	105	44.450	44	24	10	65	4.5
	6.5 to 7	110		50	28	12	65	4.5

- Tolerance between L, L₁ and L₂ is per JIS B 0405 Coarse Class
- Items with asterisk can be customized as needed.



Unit: mm

Nominal dimensions	Module (m)	Pitch diameter (d0) (approx.)	L	L ₁	L ₂	D ₁	Taper at shank section	a*	
25	0.75 to 0.9	25	80	10	40	18.0	1/20.020 0.049951	2	Morse taper No. 2
	1 to 1.5	25	80	12	40	18.0	1/20.020 0.049951	2	
	1.75 to 2.5	25	80	15	40	18.0	1/20.020 0.049951	2	
38	0.75 to 0.9	38	100	12	50	24.1	1/19.922 0.050196	2	Morse taper No. 3
	0.75 to 0.9	38	100	12	50	27.0	1/19.185 0.052125	2	Fellows taper
	1 to 1.75	38	100	15	50	24.1	1/19.922 0.050196	2	Morse taper No. 3
	1 to 1.75	38	100	15	50	27.0	1/19.185 0.052125	2	Fellows taper
	2 to 3	38	100	18	50	24.1	1/19.922 0.050196	3	Morse taper No. 3
	2 to 3	38	100	18	50	27.0	1/19.185 0.052125	3	Fellows taper
	3.25 to 4	38	125	18	50	24.1	1/19.254 0.05194	3	Morse taper No. 4
	3.25 to 4	38	125	18	50	27.0	1/19.185 0.052125	3	Fellows taper
	3.25 to 4	45	125	18	50	27.0	1/19.185 0.052125	3	Fellows taper

- Tolerance between L and L₁ is per JIS B 0405 Coarse Class •Items with asterisk can be customized as needed.

■ Precision Standard

No.	Item	Permissible value or tolerance		
		Grade		
		AA	A	B
1	Bore diameter (d)	19.050	+6	+9
			0	0
	Standard size (mm)	31.742	+4	+7
			0	+11
44.450	0	0		
	Shank deflection	3	4	5
2	Peripheral runout	7	10	15
3	Bottom surface deflection	3	4	6
4	Mounting surface deflection	5	5	7
5	Cutting face deflection	10	16	25
6	Cutting angle (min.)			
7	Side clearance angle (min.)	±10	±14	±20
8	Front clearance angle (min.)			

- For No. 1, bore diameter applies to the disc shape and bell shape, while shank deflection applies to the shank shape.

- For No.s 3 and 4, only applies to the disc shape and bell shape.

Unit: μm

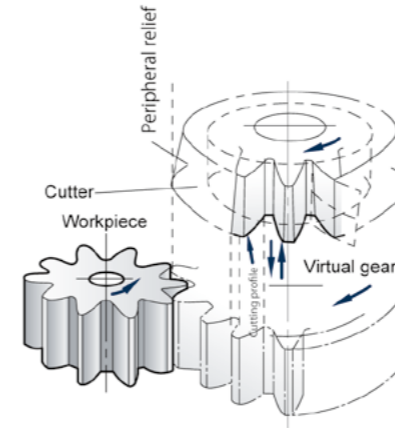
No.	Item	Grade	Nominal size	Permissible value or tolerance								
				Module (m)								
				0.75 or higher 1 or less	Over 1, 1.6 or less	Over 1.6 2.5 or less	Over 2.5 4 or less	Over 4 6 or less	Over 6 10 or less	Over 10 12 or less		
9	Runout	AA	25, 38, 50	10	10	10	11	-	-	-		
			75, 100	11	11	12	13	14	17	-		
			125, 150, 175	-	12	13	14	15	18	23		
		A	25, 38, 50	14	14	15	16	-	-	-		
			75, 100	16	16	16	18	20	24	-		
			125, 150, 175	-	18	19	20	22	26	32		
B	25, 38, 50	28	28	30	33	-	-	-				
	75, 100	31	31	33	36	40	48	-				
	125, 150, 175	-	35	37	40	45	52	65				
10	Adjacent pitch error	AA	25, 38, 50	3	3	4	4	-	-	-		
			75, 100	4	4	4	4	5	6	-		
			125, 150, 175	-	4	5	5	6	7	9		
		A	25, 38, 50	5	5	6	6	-	-	-		
			75, 100	6	6	6	7	8	9	-		
			125, 150, 175	-	7	7	8	8	10	13		
		B	25, 38, 50	10	10	12	13	-	-	-		
			75, 100	12	12	13	14	16	19	-		
			125, 150, 175	-	14	15	16	18	21	27		
		11	Cumulative pitch error	AA	25, 38, 50	10	11	12	12	-	-	-
					75, 100	12	13	13	14	15	18	-
					125, 150, 175	-	14	15	15	17	20	24
A	25, 38, 50			18	19	21	23	-	-	-		
	75, 100			21	22	23	25	28	34	-		
	125, 150, 175			-	25	26	28	32	37	46		
B	25, 38, 50			26	28	30	33	-	-	-		
	75, 100			30	31	33	36	40	48	-		
	125, 150, 175			-	35	37	40	45	52	65		
12	Profile error (*)	AA	-	4	4	5	6	8	11	16		
		A	-	8	9	10	13	16	22	32		
		B	-	16	18	21	25	32	43	63		
13	Tooth thickness (-)	AA	-	13	13	17	21	27	33	43		
		A	-	21	21	27	33	43	53	67		
		B	-	33	33	43	53	67	80	95		

- Errors in the (*) (-) sides must not exceed 1/3 of the tolerance.

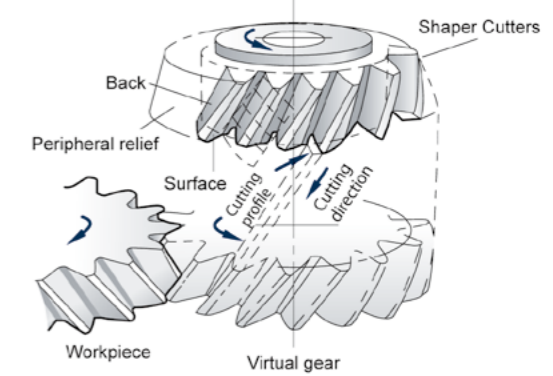
Processing by Shaper Cutters

Attach the shaper cutter to the gear shaping machine and perform gear cutting vertically from the upper to the lower section and then back to the upper section (non-cutting) in a reciprocal motion. As cutting cannot be performed during the return, it is not as efficient as hobbing, which allows continuous processing. While a helical guide is required during helical gear processing, which involves torsional motion, our lineup features the guideless ST series (NC gear shaper).

Processing spur gear with gear shaping machine



Processing helical gear with gear shaping machine

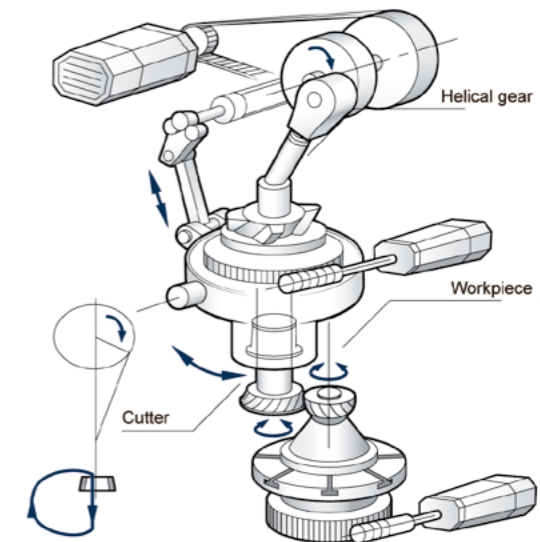


■ Gear shaping

Operate the cutter by reciprocal motion along tooth lead

- (1) Synchronous rotation of cutter and workpiece
- (2) Reciprocal motion of the cutter
- (3) Relieving motion of the cutter at returning
- (4) Feed of the cutter
- (5) Position of the cutter and the workpiece, stroke width
- (6) Other

- Cutter clamp
- Workpiece clamp, replacement, etc.

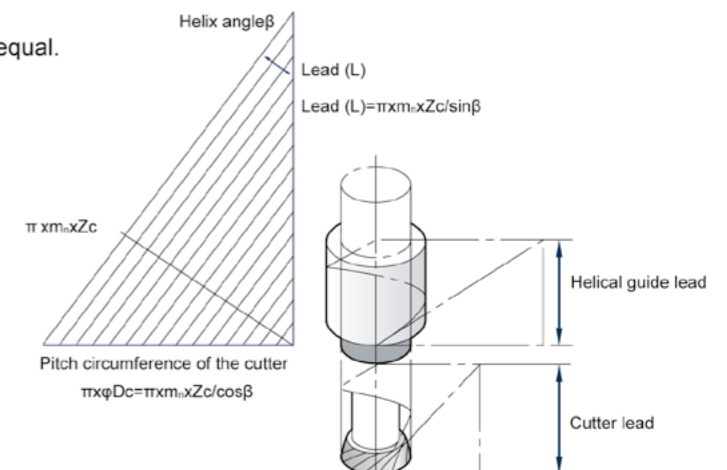


■ How to find the cutter and helical guide lead

The lead between the cutter and the guide must be equal.

$$\text{Lead (L)} = \pi \times m_n \times Z_c / \sin \beta$$

- m_n : Normal module
- Z_c : Cutter teeth number
- β : Cutter helix angle



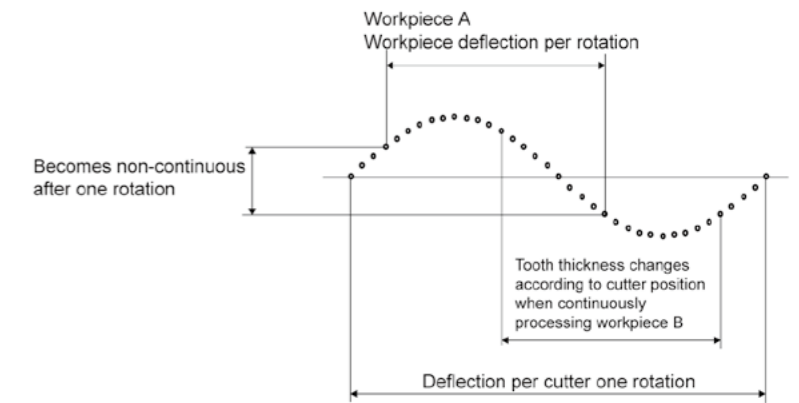
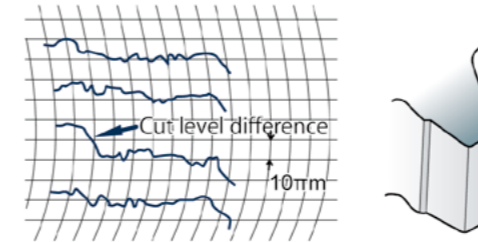
Gear Shaping Problems and Causes

	Problem	Symptom	Cause
Workpiece	Workpiece profile	Workpiece profile error	<ol style="list-style-type: none"> Poor cutter tooth profile Poor cutter face angle/sharpening angle Poor gear shaping machine precision
		Gap in one tooth	<ol style="list-style-type: none"> Poor cutter runout precision Poor cutter cumulative pitch precision
		Insufficient meshing length	<ol style="list-style-type: none"> Insufficient tooth depth Excessive cutter tip point radius Poor cutter protuberance profile
Workpiece	Cutter runout	Workpiece runout error	<ol style="list-style-type: none"> Poor cutter runout precision Poor cutter and workpiece mounting precision
		Pitch	<ol style="list-style-type: none"> Poor cutter pitch precision Poor gear shaping machine precision
Workpiece	Lead	Workpiece lead error	<ol style="list-style-type: none"> Poor gear shaping machine precision Insufficient workpiece rigidity Poor workpiece mounting jig precision Insufficient workpiece mounting jig rigidity
			Chamfering
Workpiece	Chamfering	Difference in chamfering amount by the sides	<ol style="list-style-type: none"> Poor cutter chamfering height
		Gap in chamfering section	<ol style="list-style-type: none"> Insufficient tooth depth due to excessive run-in at chamfering section of helical shaper cutter
Workpiece	Tear	Tear in workpiece	<ol style="list-style-type: none"> Flaking at the root of helical shaper cutter Excessive run-in at sharpening face of helical shaper cutter Sticky work material Improper cutting conditions: Improper or deteriorated cutting oil Relieving interference
			Major fractures
Cutter	Fractures	Abnormal wear	<ol style="list-style-type: none"> Cutter workpiece material defect Insufficient hardness Poor PVD processing Angularity in the joint tip radius Items 2, 4, 5, 6, 7 in the fracture causes above may trigger abnormal wear Cutting oil ran out
			Abnormal wear

Cut Level Irregularity

● Large deflections during cutter mounting will cause discontinuity in the processed work after one rotation.

Causes tooth profile irregularity.
Irregular OBD due to incision depth changing.



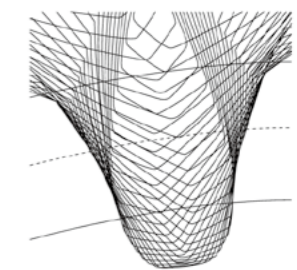
Causes of Profile Errors

- Deflection of cutter tooth will lead to poor profile precision.
- A lack of smoothness of cutter or workpiece rotation will cause mismatches in the generation position and lead to deterioration of profile precision.

Factors likely to change the cutting resistance of the biting:

- Unevenness cutter teeth balance (sharpening angle setting, uneven wear etc.)
- Error in the rotation precision of the master worm wheel (mounting error, uneven wear etc.)

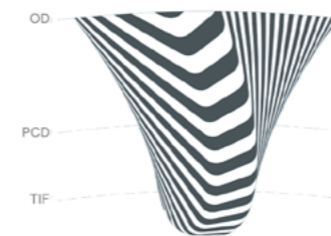
(Reference) Diagram of gear cutting processing



Profiles near the left and right points in the pitch circle are not generated at the same time.

Conventional Method of Processing and High Circumferential Feed

Conventional processing



Load concentrated on the edge in the conventional method while in the opposite side thin and long chips are removed so that cutter becomes easily worn.

High circumferential feed is effective for extending cutter life



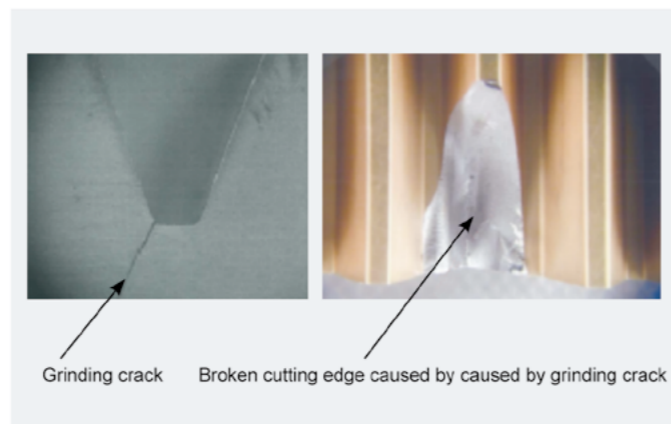
High circumferential feed means chips are removed thickly, so cutting teeth are distributed evenly, reducing wear.

Relationship Between Sharpening Face Roughness and Tool Life

● Cutter tooth roughness does not just shorten the life of the tool, but also causes fractures in the tooth due to grinding burns or cracks.

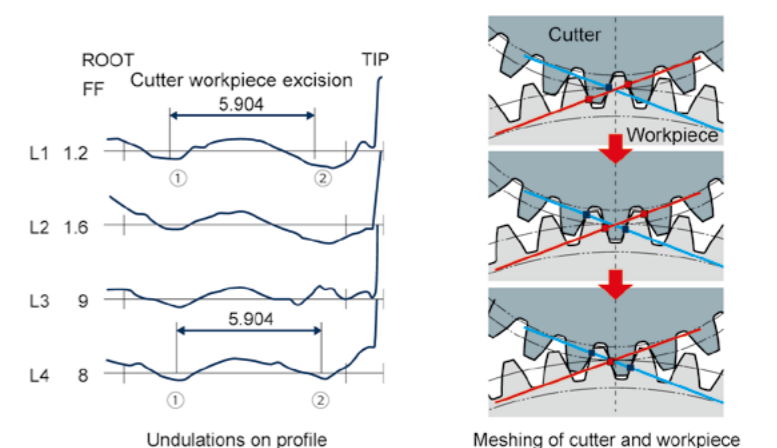


Cutter : m 1.75 NT 91
HSS
Workpiece: NT22, Width 8
SPUR
18CrMo4
HB 180
Conditions: 750/1124 str./min.
(33/50./min.)
f = 1.02/0.38mm/str.



Profile Undulations in Gears with Few Teeth

- Gears with few teeth will decrease the contact ratio and increase load changes. This will cause the cutter and workpiece to shift, leading to tooth profile undulations.
- Reduce the cutting load to reduce tooth profile undulation.



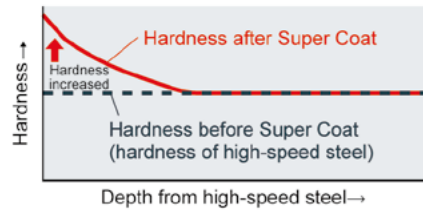
SHAVING CUTTERS

Shaving cutters are used for shaving off tiny amounts of the gear tooth surface after processing with hob or shaper cutters. Of the four types of processing (1. Conventional, 2. Diagonal, 3. Underpass, 4. Plunge cut), plunge cut is frequently used in production lines for automobile and

motorbike gears due to its efficiency and long life. Our lineup of Super Coat Shaving Cutter, Hard MACH3 Shaving Cutter, and Fine Pitch Shaving Cutter offer superior performance thanks to improvements to tool life and workpiece teeth precision.

Super Coat Shaving Cutter

- Features**
- Surface hardness increased 1.5 times over high speed steel, improving wear resistance.
 - Hardened layer: 0.1 to 0.2 mm. Almost identical surface condition.

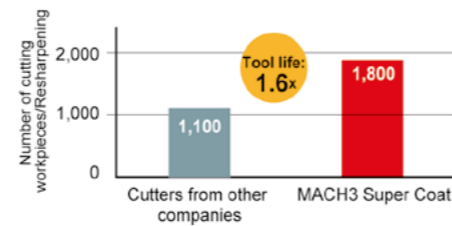


Minimizes size changes and prevents serration depth variance.

Example

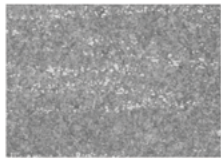
Workpiece: m2.7 PA20° HA28° RH NT68 ODφ116 Tooth width 36
Material SCr420H

Cutter: NT79 ODφ225 Material MACH3 With Super Coat



MACH3 Hard High Speed Steel

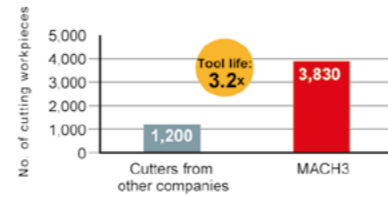
- Features**
- Increased V. Co which helps prevent wear and micro-granularized carbides dispersed throughout to improve toughness (chipping resistance).
 - Equalization and dispersal of carbides to give hardness and ensure grindability is unchanged.



Example

Workpiece: m1.75 PA17.5° HA34° LH NT43 Tooth width 12.5
Material SCr420H

Cutter: NT97 HA19° RH Material MACH3 Plunge



Fine Pitch Shaving Cutter

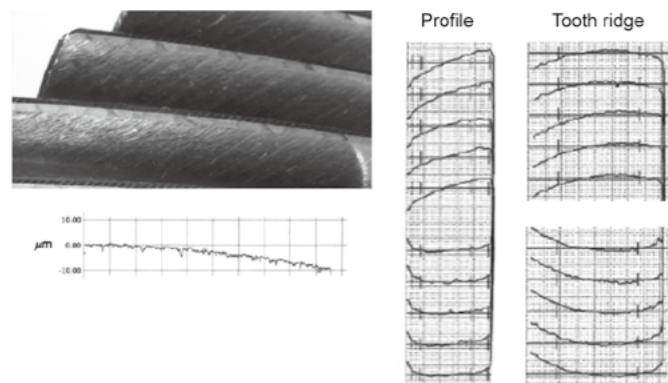
- Features**
- Reducing serration pitch spacing to smaller than standard improves tooth face roughness.
 - Optimized pitch size based on original design simulations to create high-precision tooth profiles.

Example

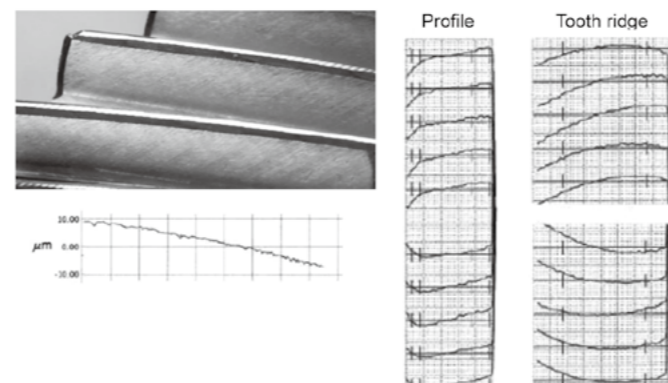
Extension of tool life and cost reduction with fine pitch + material change + Super Coat SVC

Workpiece: m1.7 PA17.5° HA36° NT45° Cutter: NT113 HA21° Improvement measures: High rigidity, fine pitch, super coating
Cutting conditions: Rotational speed 220 rpm, feed amount 0.4 mm/min. T₁:2 T₂:4 T₃:4 BM: 0.02 Plunge

Processed tooth surface with SVC of other manufacturer (wear after processing 1500 units)

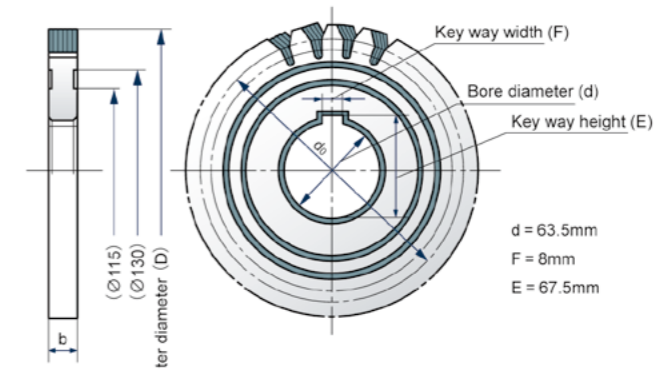


Processed tooth surface with Fine Pitch SVC (wear after processing 5500 units)



Dimensions and Precision Standard

■ Dimensions



Nominal size	Module (m)		Width b	Reference		
	Series			Standard diameter d ₀	m×z	No. of teeth z
175	1	1	19.05 25.4	175	179.0	179
		1.25			176.6	157
	1.5	1.375			179.1	137
		1.75			176.7	127
	2	2			179.2	113
		2.25			176.8	97
	2.5	2.5			179.3	89
		2.75			176.9	79
	3	3			167.5	67
		3.5			167.8	61
	4	4			177.0	59
		4.5			164.5	47
200	1	1	19.05 25.4	200	197.0	197
		1.25			201.4	179
	1.5	1.375			196.3	157
		1.75			204.9	149
	2	2			205.5	137
		2.25			197.8	113
	2.5	2.5			194.0	97
		2.75			200.3	89
	3	3			197.5	79
		3.5			200.8	73
	4	4			201.0	67
		4.5			206.5	59
5	5	188.0	47			
	5.5	193.5	43			
225	1.25	1.25	19.05 25.4	225	205.0	41
		1.375			203.5	37
	1.5	1.5			186.0	31
		1.75			223.8	179
	2	2			215.9	157
		2.25			223.5	149
	2.5	2.5			222.3	127
		2.75			226.0	113
	3	3			211.7	97
		3.5			222.5	89
	4	4			217.3	79
		4.5			219.0	73
5	5	213.5	61			
	5.5	212.0	53			
6	6	211.5	47			
	7	215.0	43			
8	8	225.5	41			
			222.0	37		
		217.0	31			
		232.0	29			

Unit: mm

Nominal size	Module (m)		Width b	Reference		
	Series			Standard diameter d_0	$m \times z$	No. of teeth z
	1	2				
300	1.5	1.75	31.75	300	268.5	179
		2			274.8	157
	2	2.25			298.0	149
		2.5			285.8	127
	2.5	2.75			282.5	113
		3			294.3	103
	3	3.5			291.0	97
		4			276.5	79
	4	4.5			292.0	73
		5			301.5	67
	5	5.5			295.0	59
		6			291.5	53
6	7	282.0	47			
	8	287.0	41			
8	9	296.0	37			
	10	279.0	31			
10	11	290.0	29			
	12	297.0	27			
					276.0	23

- Module series are based on JIS B 1701-2.
- The width "b" can be changed to suit the helix angle, shaving method, etc.

■ Precision Standard

Unit: μm

No.	Item	Permissible value or tolerance					
		Module (m)					
		1 or more 2 or less	Over 2 3.5 or less	Over 3.5 6.3 or less	Over 6.3 10 or less	Over 10 12 or less	
1	Outer diameter D	± 400					
2	Width b	± 200					
3	Bore diameter d	-5 0					
4	Key way	Width F	+90 0				
		Height E	+300 0				
5	Peripheral runout	15					
6	Side face deflection	5					
7	Runout	225 mm or lower	14	14	14	15	—
		300mm	18	18	19	19	20
8	Single pitch error	225 mm or lower	5	6	7	8	—
		300mm	5	6	7	8	9
	Cumulative pitch error	225 mm or lower	17	18	18	19	—
		300mm	23	23	24	24	25
9	Total profile error	225 mm or lower	2	3	4	5	—
		300mm	3	4	4	5	6
10	Tooth thickness	0 -25					
11	Tooth lead (every 25 mm)	Total lead error	7				
		Symmetry	5				

- Total profile error can be applied when modifying cutter tooth profiles as well.
- Tooth thickness shows the tolerance for the tooth thickness corresponding to the outer diameter.

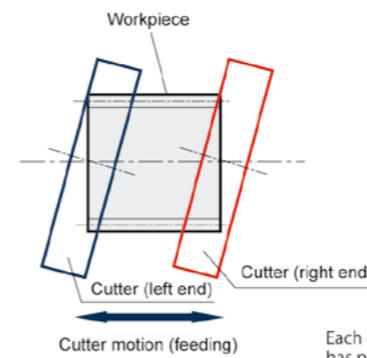
Processing Using Shaving Cutters

Adjust the crossed axes angle of a workpiece after hobbing or sharpening with a shaving cutter to between 5° to 15° and rotate after engaging the gear. The resultant sliding motion of the tooth surface enables fine finishing with only a small amount of cutting. As this is cheap and suited to mass production, it is used in the production of gears for automobiles or construction machinery. Shaving cutter processing is only possible prior to heat treatment. (Following heat treatment, use profile grinding.)

The diagrams show the interaction between a shaving cutter and a gear. The first diagram shows the cutter teeth moving across the gear teeth, highlighting the serration edge and the workpiece gear. The second diagram shows the meshing process with rotation directions and contact points. The third diagram shows the expansion of the serration edge, with labels for Root, Burr, Abrated surface, Abrasion by chip, Undercut, Tip, and Driven side. The fourth diagram is a schematic of the cutting mechanism, showing the cutter, workpiece surface, and the crossed axes angle between the cutter and gear central axes.

■ Conventional processing

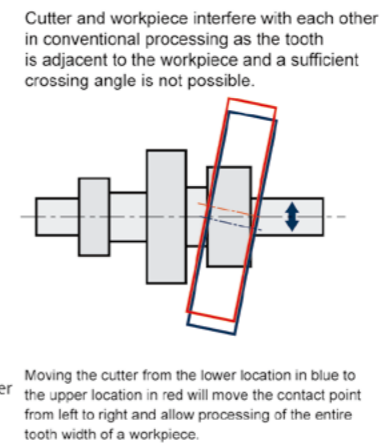
Move cutter in parallel to workpiece axis



1. Wider workpieces can be processed with narrow cutters.
2. Easy to share cutters among some different kinds of workpieces.
3. The motion of the machinery enables crowning and taper processing.
4. The cutter moves a long way compared to other methods.
5. Only the center of the cutter is used, wasting much of the tool.

■ Underpass processing

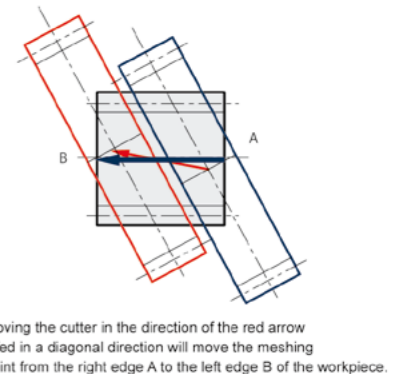
Move cutter at a right angle to workpiece axis



1. Uses a cutter wider than the workpiece tooth width.
2. Requires sharpening for underpass processing
3. Requires sharpening for hollow tooth profile for crowing processing.

■ Diagonal processing

Move cutter diagonally to workpiece axis

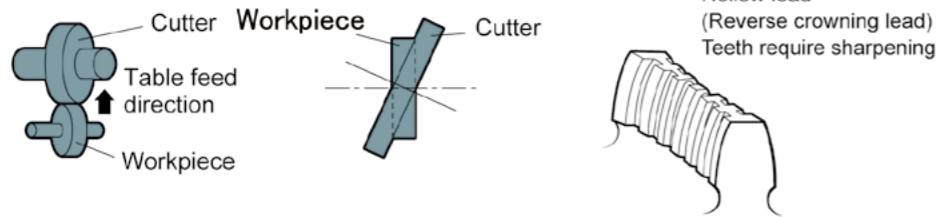


1. The cutter moves less than the conventional processing, allowing for shorter processing times.
2. The entire width of the cutter can be used, increasing its tool life.

■ Plunge processing

Does not move the cutter and workpiece during processing. Processing is only possible with a cutter that uses special sharpening.

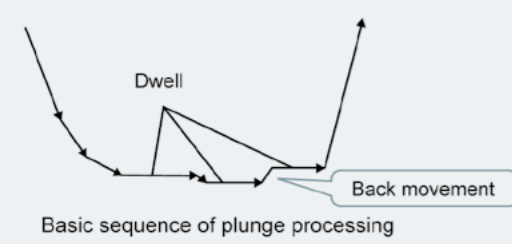
Further reduces processing time compared to other methods.



Plunge shaving processing

1. Cutter width is wider than workpiece tooth width.
2. Specially designed to match the number of teeth of a workpiece.
3. Uses differential serration.
4. Requires machine rigidity and motor power.

Setting processing conditions



Cutting speed
 Plunge, underpass: 145 m/min.
 Diagonal, conventional: 120 m/min.

Incision feeding (per workpiece rotation)
 Axis: 0.5 μm
 Hole: 1.5 μm

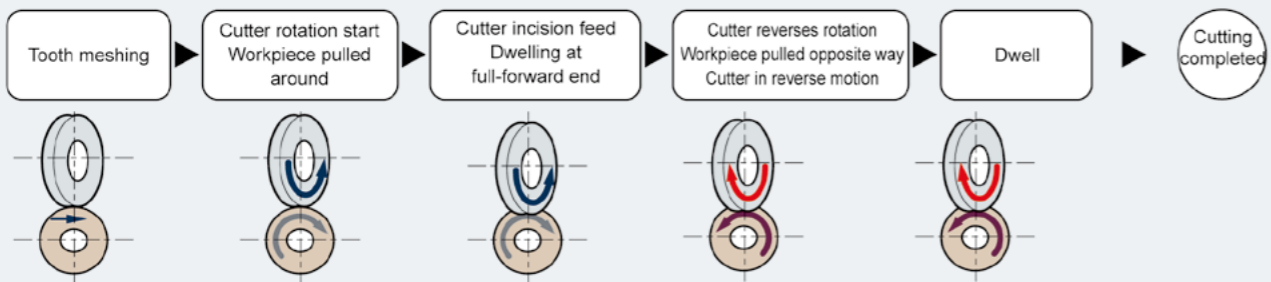
Traverse feeding (per workpiece rotation)
 Diagonal, Conventional 0.2mm
 Underpass 0.1mm

Plunge dwelling time
 Regard 35 rotations of a workpiece as the benchmark

Note
 The rotational speed of workpieces with a hole must be less than 2000 rpm.
 For workpieces with a shaft, it is less than 1000 rpm.

Sequence

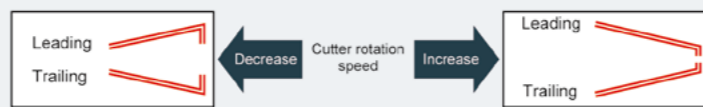
The normal shaving process is cutter-driven and the workpiece is rotated by it. Start processing after meshing the cutter and workpiece. Use the cutting teeth at both sides and switch the cutter rotation direction to ensure stable precision. In order to remove the looseness generated at incision, use dwell to ensure stable precision.



Improvement of Profile Precision

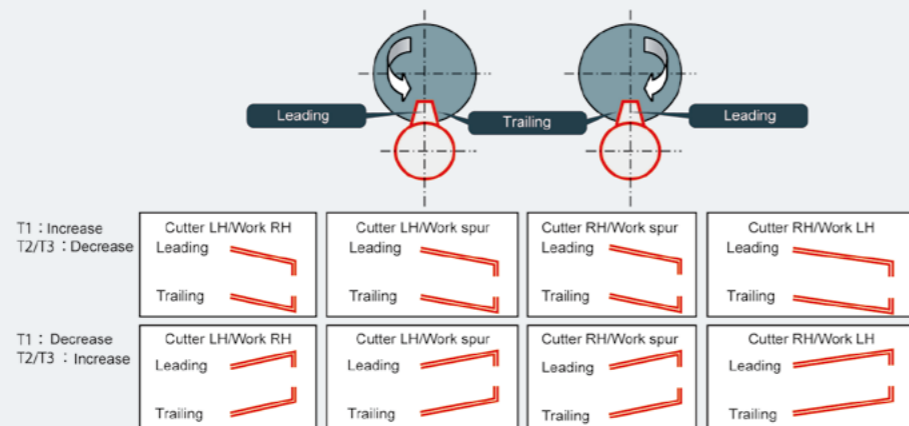
● Impact of cutter rotation speed

Adjustment is likely to cause the changes shown in the following diagram.



● Impact of dwell timer

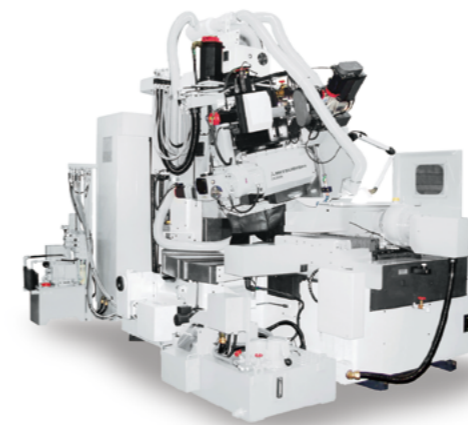
Changes the leading/trailing cutting surface depending on the cutter rotation direction.



Gear Shaving Problems and Causes

	Problem	Symptom	Cause
Workpiece	Workpiece profile error (with manufacturer trial)	Large tooth profile error of the workpiece in the same trial processing	<ol style="list-style-type: none"> 1. Different measuring machine used 2. Different measuring teeth 3. Different profile control point
		Passed trial processing by cutter manufacturer but failed trial processing by user	<ol style="list-style-type: none"> 1. Different trial machine 2. Different trial conditions 3. Different precision difference in previous process(es) 4. Measurement error of trial workpiece by manufacturer 5. Vague manufacturer pass/fail judgment trial profile 6. Measurement error of trial workpiece by user
Cutter	Cutter teeth profile error	Cutter teeth profile does not meet user's request	<ol style="list-style-type: none"> 1. Cutter teeth profile measurement error 2. Wrong cutter teeth profile (previous profile, etc.) or copied incorrectly 3. Design instructions error 4. Order instructions error
		Low number of resharpenings	<ol style="list-style-type: none"> 1. Shallow serrations <ul style="list-style-type: none"> • Difference between sides • Differences at tip or root • Circumference irregularity • Shallow overall
	Cutter life short	Workpiece teeth profile collapse	<ol style="list-style-type: none"> 1. Low cutter hardness 2. Complicated cutter teeth profile 3. Excessive shaving stock 4. Excessive workpiece hardness
Fractures	Fracture before use	Fracture before use	<ol style="list-style-type: none"> 1. Fracture due to grinding crack during tooth profile grinding 2. Cracking during heat treatment 3. Fracture during transportation and handling
		Fracture during processing workpiece	<ol style="list-style-type: none"> 1. Shoulder gear interference 2. Processing workpiece with the wrong specifications 3. Too many workpieces processed (wear) 4. Insufficient strength at cutter root 5. Improper serration alignment

Tips: Sharpening Method



ZA30A shaving cutter grinder

When the precision requirements cannot be met during shaving, the cutter is often considered to have reached the end of its life, and is resharpened.

During resharpening, ensure that worn (abraded) parts are removed properly. Check also for burrs and ensure that they are removed.

Our ZA30A shaving cutter tooth profile grinder can achieve reproducibility and ease of rearrangement while maintaining precision through numerical control.

It is important to control the number of workpieces and resharpen the tooth profile and lead of each cutter.

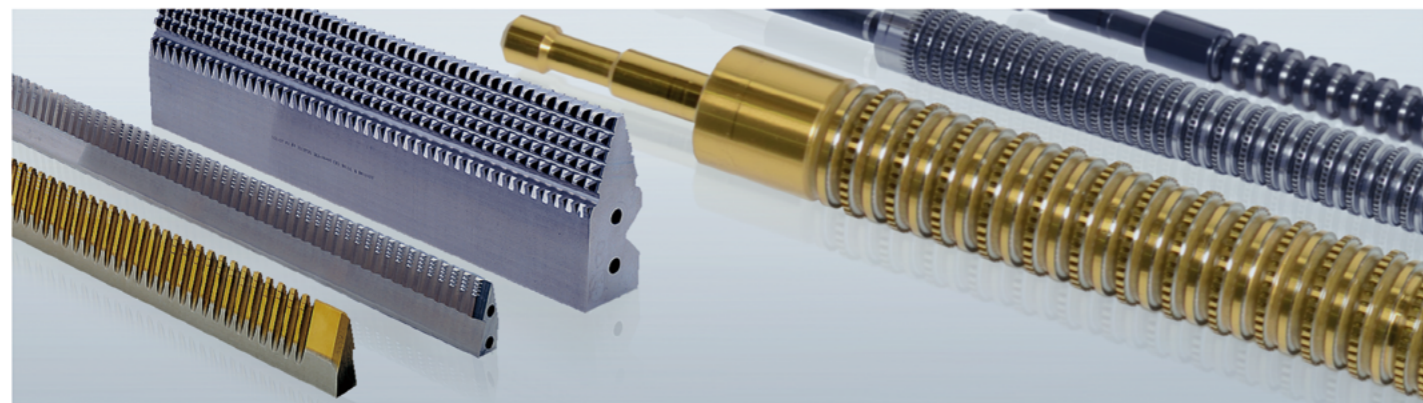
Hobs, Shaper Cutters, Shaving Cutters, Broaches, Other Products, Materials and Coatings for Tools, Estimates / Design Specifications

Hobs, Shaper Cutters, Shaving Cutters, Broaches, Other Products, Materials and Coatings for Tools, Estimates / Design Specifications

BROACHES

Broaches are divided into two groups: internal broaches for making spline holes used to process automobile reduction gears and machine tools, and surface broaches for processing the surfaces of specially-shaped parts used to make power generator and jet engine turbine

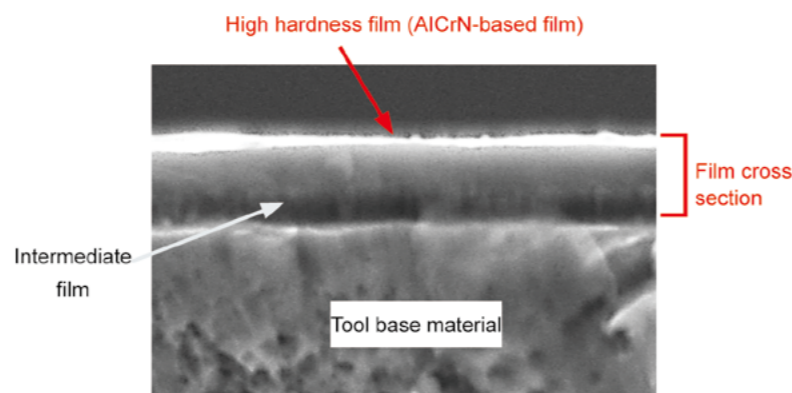
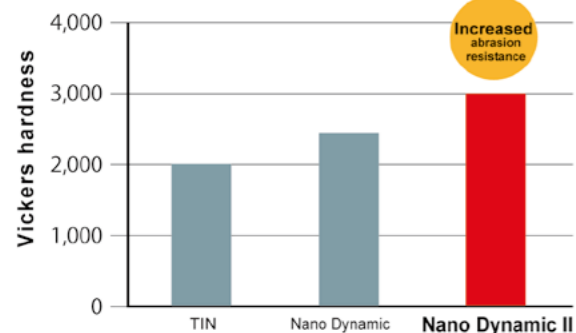
blade grooves and various industrial machinery. We design and produce a range of original broaches based on our long experience and expertise. We have a long track record of supporting the shapes and performance demanded by our customers.



Nano Dynamic II

Features

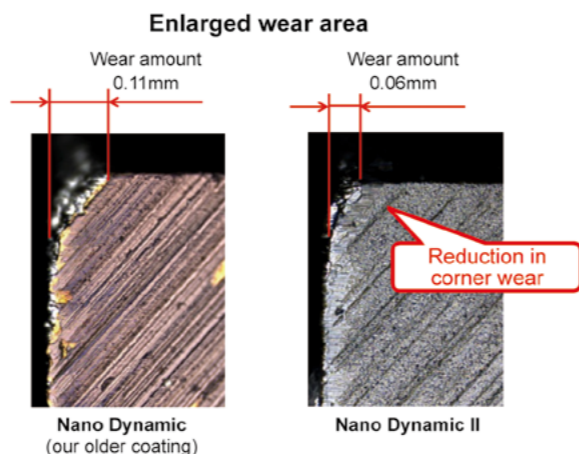
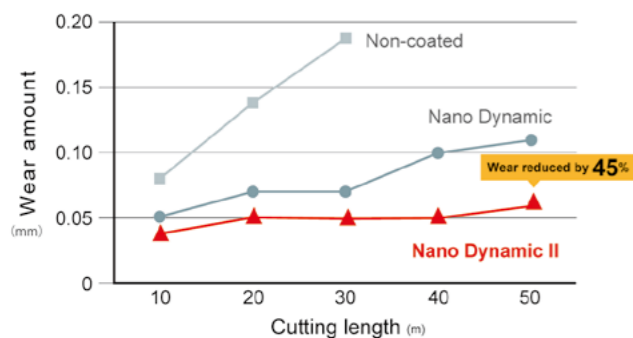
- Uses AlCrN coatings for superior heat resistance and anti-wear properties.
- Effective for dealing with corner wear of the cutting tooth.
- Effective even under conditions detrimental to tool life, such as difficult-to-cut material processing and broach cutting using water-soluble coolant.



Structure of Nano Dynamic II
Super-hard film with excellent wear resistance and an intermediate layer with excellent adhesion to the base material.

Example

Workpiece: Material S50C (hardness HB260)
Processing conditions: Cutting speed 5m/min. Cutting length 50m Oil coolant



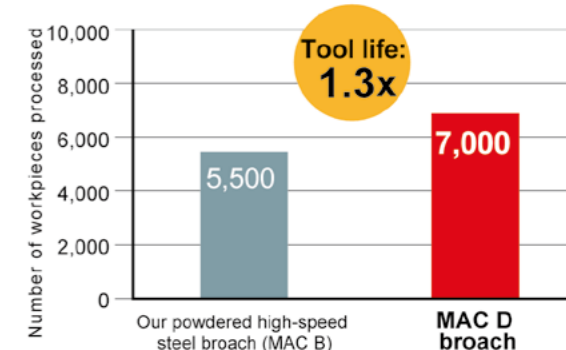
MAC D Long-Life Broach

Features

- Uses MAC D powder high-speed steel which contains high levels of VC carbides for superior wear resistance.

Example

Workpiece: ODφ90 7 grooves (groove width 10 × depth 4 × tooth width 15)
Material S55C
Cutter: Pot Broach



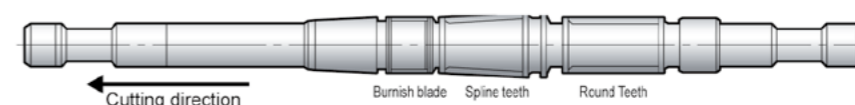
Eccentricity Preventing Broach

Features

- Increased tooth fit by prioritizing burnish teeth.

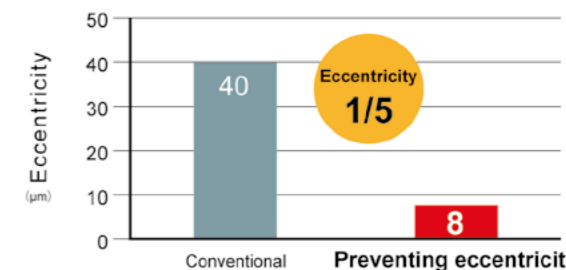
Previously: Spline teeth → Round teeth

Eccentricity-preventing broach: Burnish teeth → Spline teeth → Round teeth



Example

Workpiece: Tooth width 19.5mm Material SCM420H
Cutter: Involute spline broach ODφ33 NT32 Coating TiN
Cutting conditions: Cutting speed 5m/min.

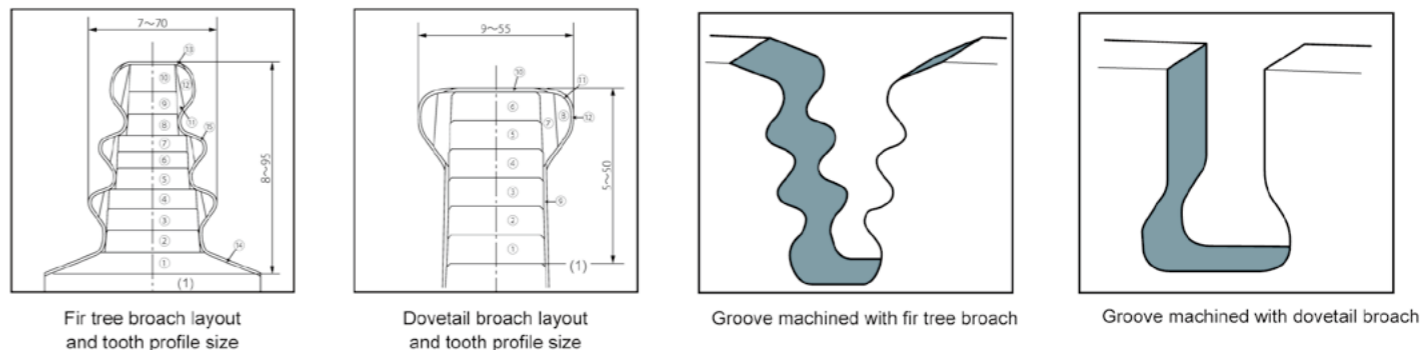


Fir Tree Broach

Features

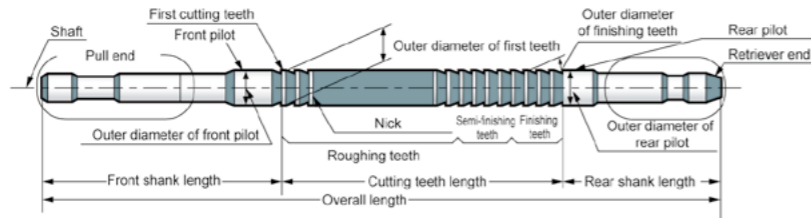
- Long tool life achieved by adopting high-alloy powder high-speed steel for difficult-to-machine materials.
- High reliability ensured by a dedicated line equipped with an advanced NC gear grinding machine and sharpening machine

Examples

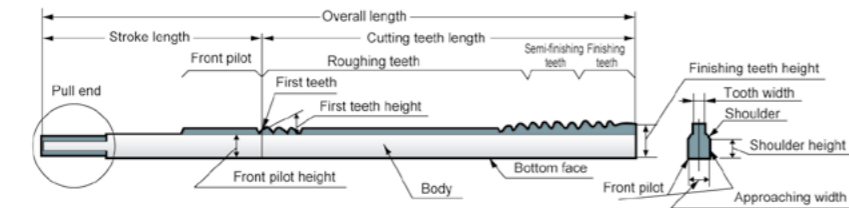


Names of Broach Parts

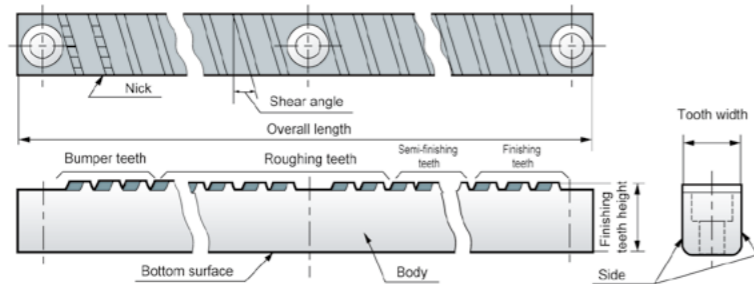
Internal broach



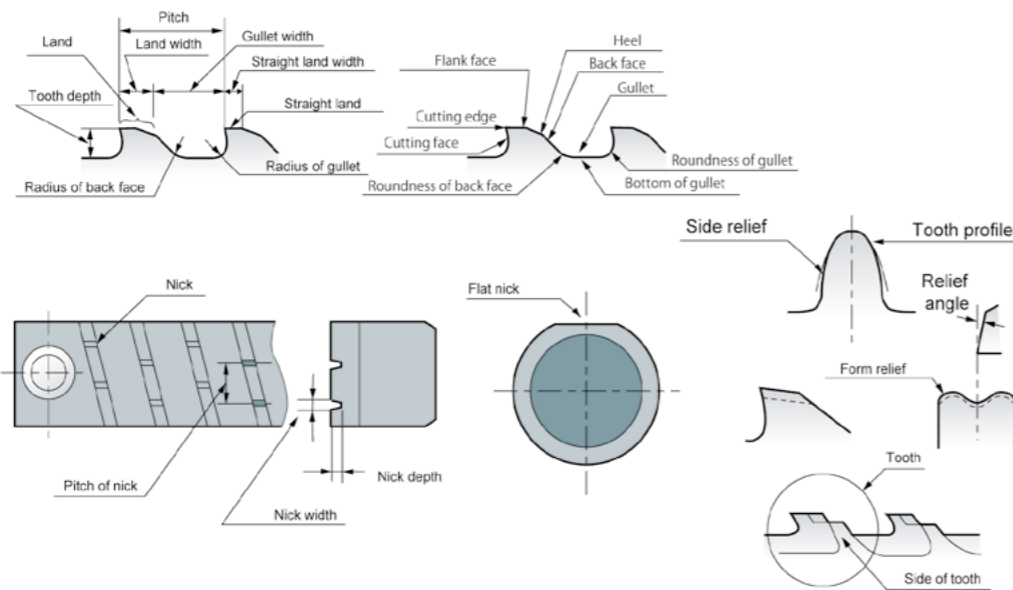
Keyway broach



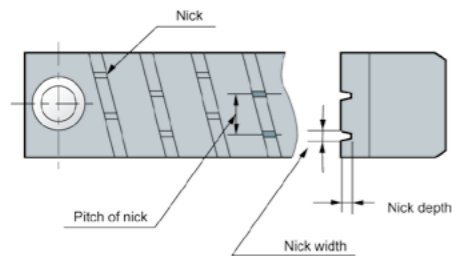
Surface broach



Teeth



Nick and relief



Cutting Methods

Cutting method	Features	Usage
Extending outward radially or upward	Leaves a constant form land, so is easy to weld, but there is no change in tooth thickness due to resharping. Also, tooth profile deformation can be reduced because the teeth fit the workpiece well.	General broaches
Extending outward and sizing radially or upward (double-cut)	Has a small cutting force for finishing tooth profile so processing distortions are reduced. Particularly effective for thin workpieces.	Fir Tree Broach Broaches for high-precision use
Back taper	The thickness of the teeth at the rear end of broach is slightly smaller and there is a tiny relief on the side of the broach tooth profile that improves cutting performance and prevents adhesion.	Broaches for long cutting lengths Broaches for workpieces prone to adhesion
Increasing tooth thickness or form	Broach tooth profile can be accurately transferred to workpiece, allowing high tooth profile precision and improved finished surface roughness.	Broach for gears Broach for high-precision use

● The concentric circle stripes indicate the order of the machining process.

Types of Broaches with Round Teeth

Type	Cutting method	Features
Spline broach with front round teeth	Machining with involute spline broach with front round teeth	If the pilot hole is precise enough, the pilot hole and spline groove concentricity improves. Simple broach structure
Spline broach with round rear teeth	Machining with involute spline broach with round rear teeth	Standard broach with round teeth
Spline broach with alternating round teeth	Machining with spline broach with alternating round teeth	Used when high concentricity of spline tooth grooves and a small diameter is required.
Spline broach with front round teeth and alternating round teeth	Machining with spline broach with alternating round teeth	Used when high concentricity of spline tooth grooves and a small diameter is required, and decentering from the pilot hole is not desired. However, if the pilot hole precision is low, decentering may become larger than using a spline broach with alternating round teeth.

• Numbers such as (1) and (2) indicate the order of the machining process.

Workpiece Hardness

The hardness of a workpiece suitable for broaching is generally HB200 to 230 (HRC14 to 21), although up to HB300 (HRC32) is often used. Excessively soft steel may cause adhesion on the side of the tooth or the land resulting in a low finished surface quality, with tears or flaking. Workpieces harder than HB300 may shorten the life of the broach.

Cutting Speed

Cutting speed has an impact on both broaching accuracy and tool life. Use the recommended values for each material shown below as the guide to determine the cutting speed.

Workpiece material		Unit: m/min
Steel		3 to 8
Stainless steel	Tough-cutting (Martensite and austenite)	2.5
	Free-cutting (Ferrite)	6 to 8
Cast iron		10
Brass		10
Bronze		10
Aluminum		10
Magnesium		10

Calculation of Drawing Force F

$$F = f \times n \times Q \text{ (kgf)}$$

f = Cutting resistance per unit (kgf/mm²)

n = Number of teeth simultaneously used for cutting (pieces)

Q = Total cut area per tooth (mm²)

(1) Calculating cutting resistance per unit f

Steel Hardness	Unit: kgf/mm ²
Up to HRC30	300
HRC30 to HRC35	350
HRC35 to HRC40	400
Malleable cast iron	200
Cast iron, bronze, aluminum	100

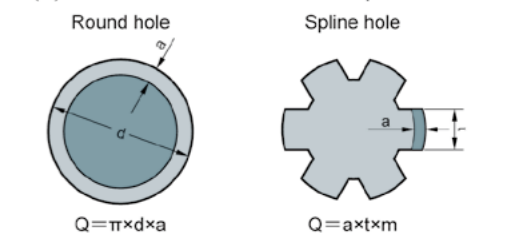
(2) Calculation of number of teeth simultaneously used for cutting n

$n = \ell/P$ (pieces)
All values are rounded up to the nearest integer.

ℓ = Workpiece thickness (mm)

P = Broach tooth pitch (mm)

(3) Calculation of total cut area per tooth Q



d = Broach external diameter (mm)

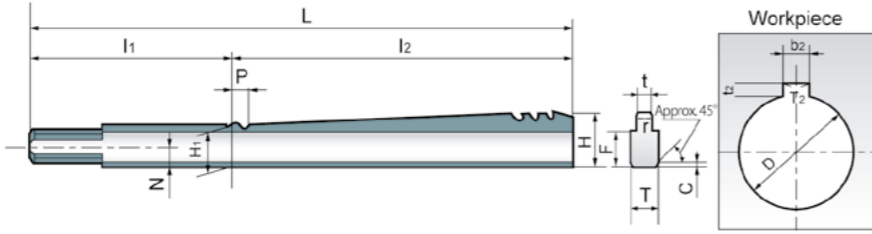
t = Cutting width per tooth (mm)

m = Number of spline grooves (grooves)

a = Machining allowance per broach tooth (mm)

Dimensions and Precision Standard

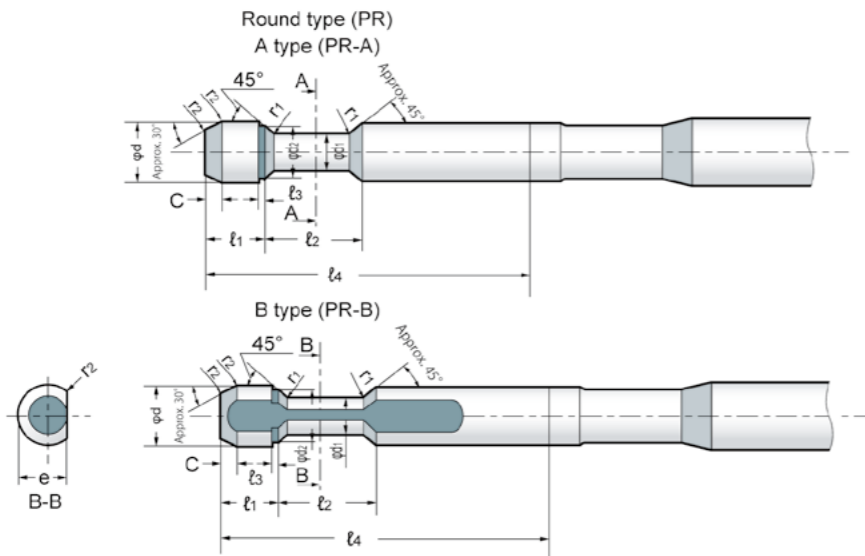
Keyway broach shape and dimensions



Bearing No.	Standard size	Edge width t			Broach width T		Finishing teeth height H	1st tooth height H1	Overall length L	Shank height I1	Cutting teeth length I2	Shoulder height F	Chamfering C
		Tolerance			Standard size	Tolerance h7							
		For sliding type D10	For standard type JS9	For clamping type P9									
310016	3	+0.012	-0.006	+0.060	5	0	9	7.27	425	165	260	6	0.5
310028		-0.002	-0.020	+0.046			8	7.13	530	185	345	5	
310045-2							9	6.68	475	220	255	5.5	
410028	4	+0.015	-0.012	+0.078	5	-0.012	8	6.84	500	220	280	4.5	0.5
410045-2		-0.003	-0.030	+0.060			10	7.76	710	225	485	6	
412045							9	7.88	600	265	335	5	
412063-2	5	+0.015	-0.012	+0.078	7	0	11	8.10	630	190	440	6.5	0.8
513028		-0.003	-0.030	+0.060			10	8.55	670	265	405	5.5	
513063-2							13	10.17	800	230	570	8	
515045	6	+0.015	-0.012	+0.078	8	-0.015	12	10.58	750	320	430	7	1
515090-2		-0.003	-0.030	+0.060			16	12.59	850	230	620	10	
618045							14	12.29	1,000	270	730	8	
618063	8	+0.018	-0.015	+0.098	12	0	21	16.81	950	240	710	13	1.2
618112-2		-0.003	-0.030	+0.060			19	16.90	850	330	520	11	
824045							25	21.64	1,120	430	690	17	
824063	10	+0.018	-0.015	+0.098	15	-0.018	26	21.64	900	240	680	17	1.5
824090-2		-0.004	-0.037	+0.076			23	20.82	1,250	330	920	14	
824140-2							29	26.79	1,250	510	740	20	
1030045	12	+0.021	-0.018	+0.120	17	0	32	27.58	950	250	700	23	1.5
1030090		-0.004	-0.037	+0.076			34	28.88	1,250	340	910	20	
1030112-2							29	26.79	1,000	385	615	24	
1030180-2	14	+0.021	-0.018	+0.120	19	-0.021	31	28.44	1,250	520	730	21	2
1240045		-0.006	-0.045	+0.093			35	30.19	1,060	250	810	25	
1240090							33	30.09	1,400	340	1,060	22	
1240112-2	16	+0.021	-0.018	+0.120	19	0	36	30.19	1,060	250	810	25	2
1240180-2		-0.006	-0.045	+0.093			33	30.09	1,400	385	675	22	
1445045							33	30.09	1,400	520	880	22	

- The pull and retriever ends are per the screw types specified in JIS B 4237.
- Tolerances of L, I1 and I2 are ±5mm.
- Tolerances of H and H1 are 0 mm and 0 mm respectively.
- Tolerance of N is the medium class specified in JIS B 0405.

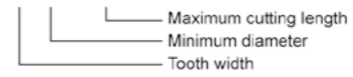
Shape and dimensions of pull end of broach (round type)



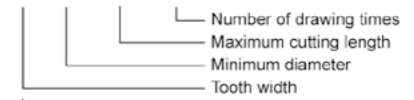
(1) The bearing number shows the tooth width, minimum diameter of workpiece, and maximum cutting length, in that order.

"-2" at the end of the bearing number means that it draws twice.

Example 1. **3 1 0 0 1 6**



Example 2. **1 2 4 0 1 1 2 -2**



(2) The estimated load is generally calculated with the following formula.

Estimated load = (Cutting width) x (Cutting amount per tooth) x (Cutting resistance per unit) x (Number of teeth simultaneously used for cutting)

Next is an example of when the work cutting resistance per unit is 294 kPa.

Example: If the bearing number is 1240045, the estimated load is $12 \times 0.08 \times 2.94 \times 5 = 14 \text{ kN}$

Unit: mm

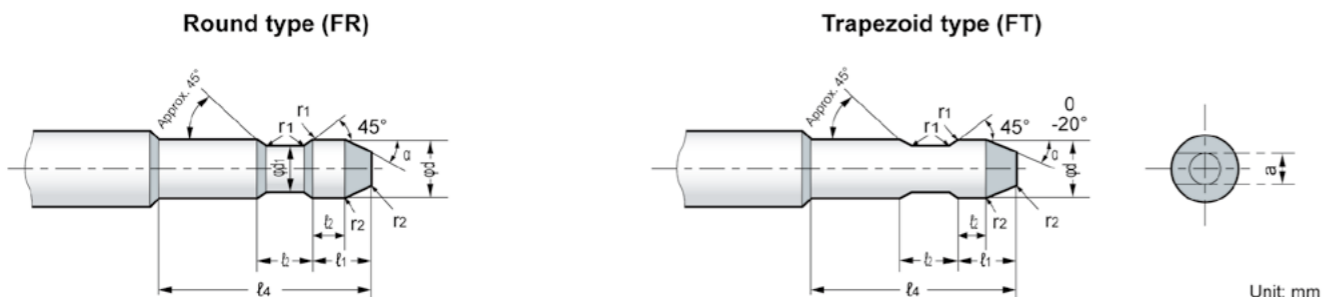
Edge corner radius r	H-H1	Pitch P	Pull end nominal size N	Height to center of screw	Workpiece dimensions (reference values)				Use conditions (for reference)										
					Keyway width b2	Keyway depth t2	Corner radius r2	Minimum diameter D	Maximum cutting length	Number of drawing times	Stroke	Estimated load kN							
0.08 ~ 0.16	1.73	6	6	3.5	3	1.4	0.08 ~ 0.16	10	16	1	330	1							
									28	1	440	2							
									45	2	380	2							
					4	1.8			10	28	1	510	3						
										45	2	400	3						
										63	2	500	4						
0.16 ~ 0.25	2.9	8	8	4.5	5	2.3	0.16 ~ 0.25	13		28	1	530	4						
										63	2	570	5						
										90	2	640	6						
					6	2.8			10	6	8	8	3.3	18	45	1	740	6	
															63	1	890	7	
															112	2	790	9	
0.25 ~ 0.4	4.36	10	16	11	10	3.3	0.25 ~ 0.4	30							45	1	780	11	
															90	1	1,130	16	
															112	2	830	18	
					4	2.0			18	13	12	3.3	40	180	2	1,130	23		
														45	1	820	14		
														90	1	1,120	19		
6	2.1	20	15	14	3.8	45	112	2						870	22				
							180	2						1,190	27				
							45	1						870	18				
0.25 ~ 0.4	5.12						14	20	15	16	4.3	50	90	1	1,120	22			
													112	2	990	25			
													180	2	1,370	32			
		8	2.56	10	20	15							16	4.3	50	45	1	930	21
																90	1	1,270	29
																112	2	930	30
10	2.91	16	20				15	16	4.3	50	180	2				1,270	41		

● r is per r2 of the keyway dimensions in JIS B 1301.

Nominal size	Shank diameter d		Neck diameter d1		Flat face height e		Head length l1	Neck length l2	Effective shank length l3 (minimum)	Flat face length l4 (minimum)	Reference					
	Standard size	Tolerance	Standard size	Tolerance	Standard size	Tolerance					d2	l5	c	r1	r2	s (mm ²)
8	8	-0.013	6	-0.080	6.5	-0.025	12	20	90	60	7.8	1	2	0.4	1	27.1
(9)	9	-0.013	6.8	-0.080	7.4	-0.025	12	20	90	60	8.8	1	2	0.4	1	35.1
10	10	-0.013	7.5	-0.080	8.25	-0.025	14	22	100	65	9.8	1	3	0.4	1	42.9
(11)	11	-0.016	8.2	-0.170	9.1	-0.047	14	22	100	65	10.8	1	3	0.4	1	51.5
12	12	-0.016	9	-0.080	10	-0.025	14	22	100	65	11.8	1	3	0.4	1	62.2
(14)	14	-0.016	10.5	-0.095	11.75	-0.032	16	25	110	75	13.7	2	4	0.6	1	85.1
16	16	-0.016	12	-0.095	13.5	-0.032	16	25	110	75	15.7	2	4	0.6	1	111
(18)	18	-0.016	13.5	-0.095	15.25	-0.032	16	25	110	75	17.7	2	4	0.6	1	141
20	20	-0.016	15	-0.205	17	-0.059	18	28	125	85	19.7	2	5	0.6	1	175
(22)	22	-0.020	16.5	-0.205	18.75	-0.073	18	28	125	85	21.7	2	5	0.6	1	212
25	25	-0.020	19	-0.110	21.5	-0.040	18	28	125	85	24.7	2	5	0.6	1	281
(28)	28	-0.020	21	-0.110	24	-0.040	20	32	140	95	27.6	3	6	1	1.6	344
32	32	-0.025	24	-0.110	27.5	-0.040	20	32	140	95	31.6	3	6	1	1.6	450
(36)	36	-0.025	27	-0.240	31	-0.073	20	32	140	95	35.6	3	6	1	1.6	570
40	40	-0.025	30	-0.240	34.5	-0.089	25	40	160	110	39.5	3	8	1	2.5	704
(45)	45	-0.025	34	-0.280	39	-0.089	25	40	160	110	44.5	3	8	1	2.5	905
50	50	-0.025	38	-0.120	43.5	-0.050	25	40	160	110	49.5	3	8	1	2.5	1130
(56)	56	-0.025	42	-0.130	48.5	-0.050	32	50	180	130	55.4	3	10	1.6	4	1380
63	63	-0.030	48	-0.130	55	-0.060	32	50	180	130	62.4	3	10	1.6	4	1810
(70)	70	-0.030	53	-0.290	61	-0.106	32	50	180	130	69.4	3	10	1.6	4	2200
80	80	-0.036	60	-0.330	69.5	-0.106	40	63	200	150	79.2	3	12	1.6	6	2820
(90)	90	-0.036	68	-0.150	78.5	-0.060	40	63	200	150	89.2	3	12	1.6	6	3630
100	100	-0.036	75	-0.150	87	-0.072	40	63	200	150	99.2	3	12	1.6	6	4410

- The value of S is the B-B cross-sectional area of B type and calculated with the standard sizes of d, d1 and e.
- Values in parentheses should be avoided as much as possible.
- Tolerances of l1 and l2 are the rough class specified in JIS B 0405.
- l4 and l5 show the values when d and e satisfy their tolerable ranges respectively.

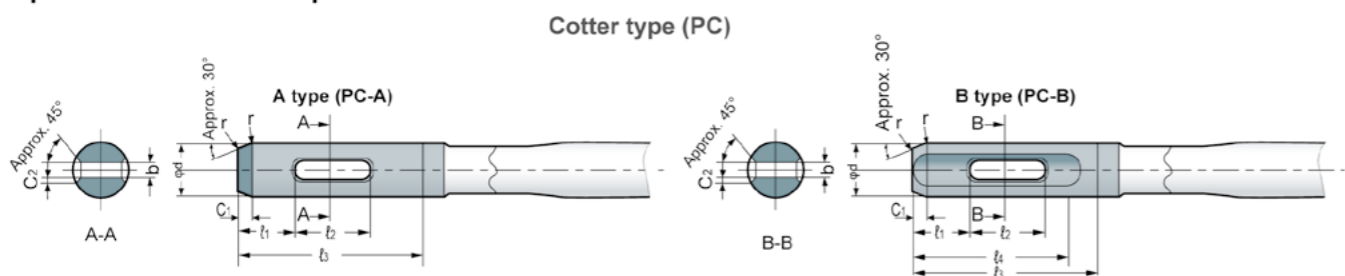
■ Shape and dimensions of retriever end of broach



Nominal size	Shank diameter d		Neck diameter or flat face width d ₁ or a		Head length Length to mounting groove l ₁	Neck length Mounting groove length l ₂	Effective shank length l ₃ (minimum)	Reference			
	Standard size	Tolerance	Standard size	Tolerance				l ₃	r ₁	r ₂	α
12	12	-0.016 -0.043	9	-0.080 -0.170	16	16	60	8	0.4	1	10°
16	16	-0.016 -0.043	12	-0.095 -0.205	16	16	60	8	0.4	1	20°
20	20	-0.020 -0.053	15	-0.095 -0.205	20	20	70	10	0.6	1.6	20°
25	25	-0.020 -0.053	18	-0.095 -0.205	20	20	70	10	0.6	1.6	20°
32	32	-0.025 -0.064	24	-0.110 -0.240	25	25	80	12	0.8	2.5	20°
40	40	-0.025 -0.064	30	-0.110 -0.240	25	25	80	12	0.8	2.5	30°
50	50	-0.025 -0.064	38	-0.120 -0.280	28	32	90	16	1	4	30°
63	63	-0.030 -0.076	49	-0.130 -0.290	28	32	90	16	1	4	30°
80	80	-0.030 -0.076	66	-0.140 -0.330	32	40	110	20	1.6	6	30°
100	100	-0.036 -0.090	86	-0.170 -0.390	32	40	110	20	1.6	6	30°

● Tolerances of l₁ and l₂ are the rough class specified in JIS B 0405.

■ Shape and dimensions of pull end of broach

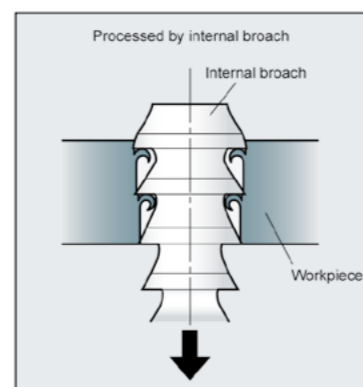


Nominal size	Shank diameter d		Cotter hole width b		Length to cotter hole l ₁	Cotter hole length l ₂	Effective shank length l ₃ (minimum)	Reference					
	Standard size	Tolerance	Standard size	Tolerance				l ₃	t	C ₁	C ₂	r	s (mm ²)
10	10	-0.013 -0.035	3	+0.4 0	16	20	70	50	9	3	0.4	1	48.6
(11)	11	-0.016 -0.043	3	+0.4 0	16	20	70	50	10	3	0.4	1	61.9
12	12	-0.016 -0.043	3	+0.4 0	16	25	70	50	11	3	0.4	1	76.9
(14)	14	-0.016 -0.043	3.5	+0.5 0	18	25	80	60	12	4	0.4	1	102
16	16	-0.016 -0.043	4	+0.5 0	18	25	80	60	14	4	0.4	1	135
(18)	18	-0.016 -0.043	4.5	+0.5 0	18	25	80	60	16	4	0.4	1	171
20	20	-0.020 -0.053	5	+0.5 0	18	25	80	60	18	4	0.4	1	212
(22)	22	-0.020 -0.053	5.5	+0.5 0	20	32	90	70	20	5	0.6	1.6	258
25	25	-0.020 -0.053	6	+0.5 0	20	32	90	70	22	5	0.6	1.6	335
(28)	28	-0.020 -0.053	7	+0.6 0	20	32	90	70	25	5	0.6	1.6	415
32	32	-0.025 -0.064	8	+0.6 0	20	32	90	70	28	5	0.6	1.6	538
(36)	36	-0.025 -0.064	9	+0.6 0	22	40	100	80	32	6	1	2.5	685
40	40	-0.025 -0.064	10	+0.6 0	22	40	100	80	36	6	1	2.5	850
(45)	45	-0.025 -0.064	11	+0.7 0	22	40	100	80	40	6	1	2.5	1080
50	50	-0.025 -0.064	12	+0.7 0	22	40	100	80	45	6	1	2.5	1350
(56)	56	-0.030 -0.076	14	+0.7 0	25	50	120	100	50	8	1.6	4	1660
63	63	-0.030 -0.076	16	+0.7 0	25	50	120	100	56	8	1.6	4	2080
(70)	70	-0.030 -0.076	18	+0.7 0	32	56	140	120	63	10	1.6	4	2570
80	80	-0.030 -0.076	20	+0.8 0	32	56	140	120	70	10	1.6	4	3360
(90)	90	-0.036 -0.090	22	+0.8 0	40	63	160	140	80	12	2.5	6	4320
100	100	-0.036 -0.090	25	+0.8 0	40	63	160	140	90	12	2.5	6	5310

● The value of S is the B-B cross-sectional area of B type and calculated with the standard sizes of d and b. However, this assumes no chamfering C₁.
 ● Values in parentheses should be avoided as much as possible.
 ● Tolerances of l₁ and l₂ are the rough class specified in JIS B 0405.
 ● l₃ shows the value when d satisfies its tolerable range.

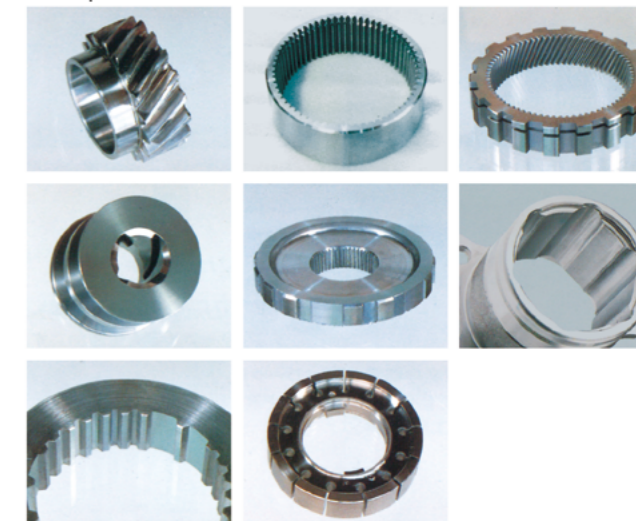
Processing Using Broaches

■ Processing using internal broaches

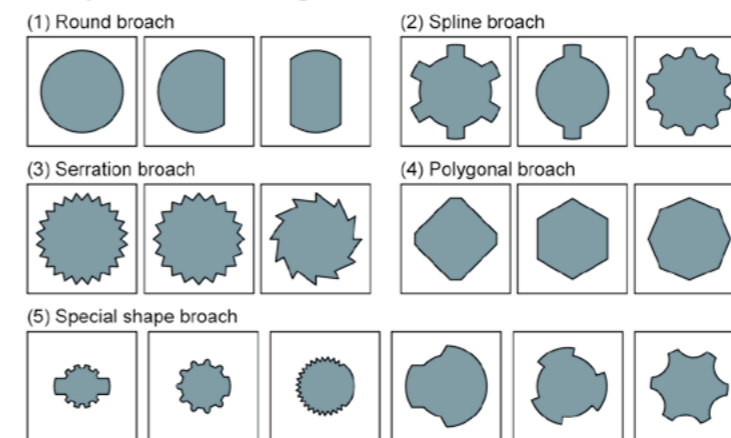


An internal broach can create the specific shape required for the internal surface of a workpiece efficiently and with high precision. Normally, the internal broach is inserted into a pilot hole which is made on the workpiece before machining. Various hole shapes can be created by selecting the optimum cutting edge shape and cutting method (for example, round, square, or polygonal, or various kinds of spline or tapered holes).

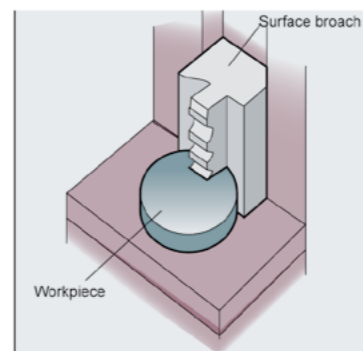
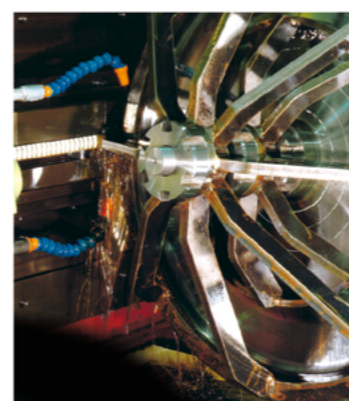
Examples



Examples of machining results

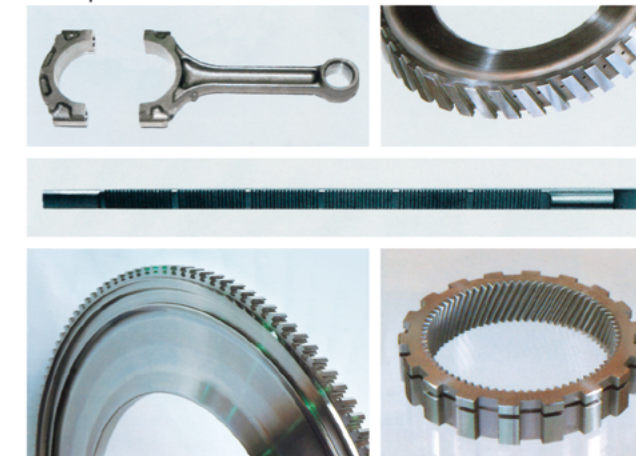


■ Processing using surface broaches

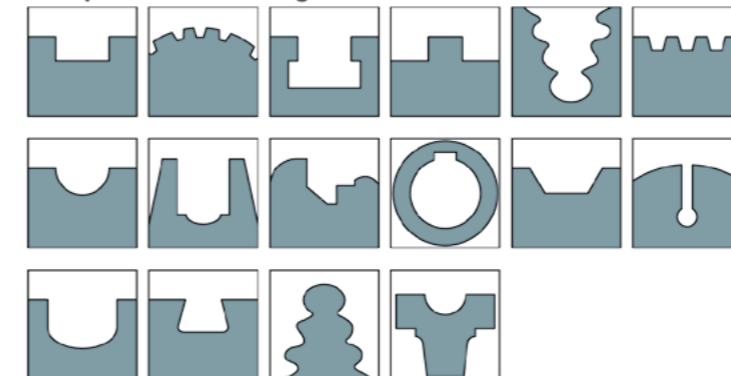


An surface broach can create the specific shape of the outer surface of a workpiece efficiently and with high precision. Roughing and finishing can be conducted at the same time, which means significantly higher productivity than milling, planing and grinding. It can machine many different shapes (for example, plane surfaces, contoured surfaces, grooves, concave-convex surfaces, gears, turbine blade roots, or turbine disc grooves) and their outline can be either as simple as a keyway or as complex such as a fir tree.

Examples



Examples of machining results



Hobs
Shaper Cutters
Shaving Cutters
Broaches
Other Products
Materials and Coatings for Tools
Estimates / Design Specifications

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How to Resharpener Broach Teeth

■ Resharpener timing

Normally, resharpen the teeth when the symptoms below show in the broach, workpiece, or broaching machine. In actuality, using the number of machined workpieces as a guide for when symptoms appear is more common.

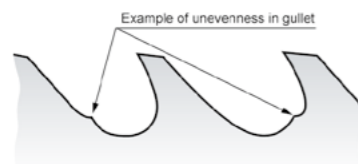
Broaches	<ul style="list-style-type: none"> Whitish land due to wearing appears on the cutting edge. Abnormal wear, chipping or cracking occurs on the cutting edge. Chips start to get stuck in the gullet.
Workpiece	<ul style="list-style-type: none"> Machined size is smaller than normal (thickness gauge cannot fit in). Machined surface is rougher than normal. Excessive heat is generated after machining.
Broaching machine	<ul style="list-style-type: none"> Cutting force is abnormally high.

■ Precautions for resharpening

Tool	<ul style="list-style-type: none"> Remove anything adhering to the cutting face. Fix any serious warping of the tool. Securely fix the tool to the sharpening machine. (If there are cracks on the cutting edge that cannot be removed by resharpening, contact us.)
Grinding wheel	<ul style="list-style-type: none"> Use a sharp CBN grinding wheel. To increase grinding efficiency, use a grinding wheel with as large a diameter as possible. Regularly dress the grinding wheel.
Grinding condition	<ul style="list-style-type: none"> Grinding amount: Grind the same amount on each tooth to remove the worn parts. Grinding rate: 1,800 to 2,000 m/mi (For internal broaches, use a workpiece rotation of about 30 m/min.)
Other	<ul style="list-style-type: none"> For internal broaches, be careful to prevent interference between the tool and the grinding wheel (see how to determine the grinding wheel angle for resharpening internal broach teeth shown to the right). Use a well-maintained sharpening machine. Make sure that the grinding fluid has not deteriorated, and supply the appropriate amount.

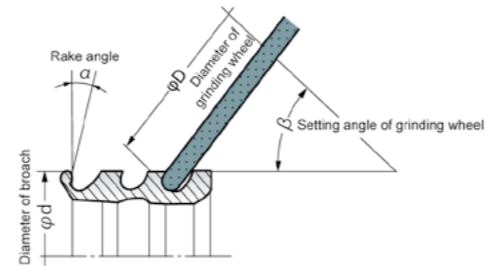
■ What to check after resharpening

- Have you completely removed all wear and cracks in the cutting edge?
- Is it free from grinding burns?
- Is the finished surface roughness no more than 3.2?
- Is there no significant unevenness in the gullet that would prevent chip expulsion?
(See figure below)
- Have you degaussed the broach?

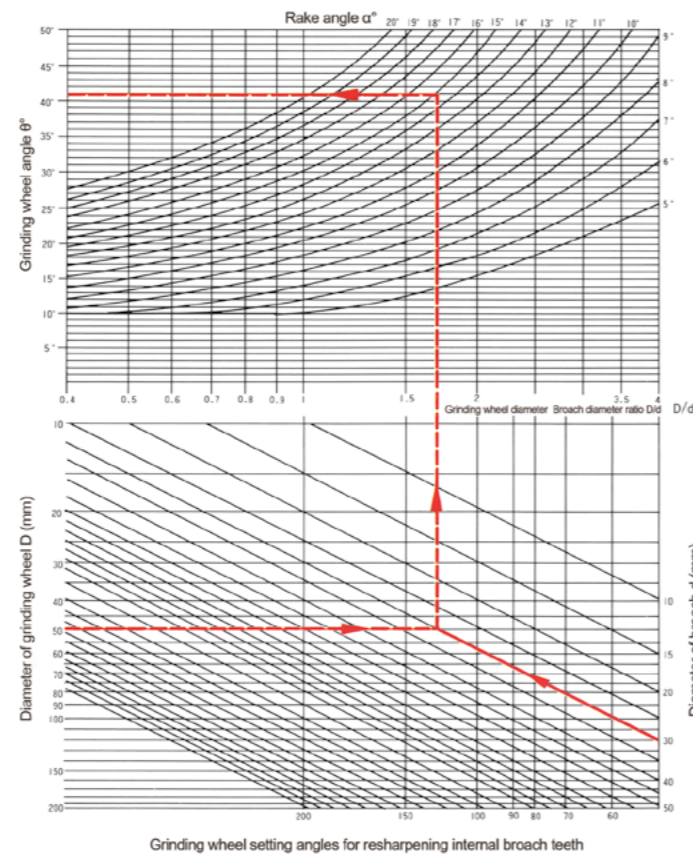


■ Grinding wheel angle for resharpening internal broach teeth

Unlike surface broaches, internal broaches cannot be resharpened correctly if the diameter and setting angle of the grinding wheel are not appropriate, as the grinding wheel and the tool will interfere with each other. See the relationship between broach shape (outer diameter and rake angle) below for reference.



If you resharpen a broach of diameter $d=30$ with a grinding wheel of diameter $D=50$ and the cutting edge hook angle is $\alpha=15^\circ$, the appropriate setting angle of the grinding wheel is $\beta=41^\circ$.



Broaching Problems and Causes

■ Internal broach

	Problem	Symptom	Cause
Workpiece	Major diameter	Major or minor diameter exceeds tolerance	1. Broach dimensions exceed tolerance 3. Flaking
	Minor diameter	Major or minor diameter below tolerance	2. Affected by burrs 3. Shrinking due to springback 4. Shrinking due to cutting heat
	Inner pin diameter	Inner pin diameter exceeds tolerance	1. Broach over-pin diameter exceeds tolerance 4. Caused by flaking 5. Caused by decentering
		Inner pin diameter below tolerance	1. Broach over-pin diameter below tolerance 4. Shrinking due to springback 5. Shrinking due to cutting heat 3. Shrinking due to poor sharpness
Machined surface	Flaking Scraping Edge chipping Chattering	1. Interference from parts other than teeth 6. Shear drop 7. Improper cutting conditions 8. Improper or deteriorated cutting oil 9. Insufficient rigidity of broaching machine 10. Difficult-to-machine workpiece	
		2. Excessive cutting allowance 3. Inappropriate face angle 4. Cutting edge is worn, cracked or chipped 5. Adhesion on side of teeth	
Decentering	The drawing hole is displaced with reference to the outer circumference.	1. Uneven circumference due to worn teeth 3. Surface contacting teeth is deflected 2. Broach is warped 4. Unbalanced cutting	
Broach	Cracked teeth	Cracked teeth	<p>Unevenness</p> <p>Gullet unevenness</p> <ul style="list-style-type: none"> Chips stuck due to faulty gullet shape Excessive land width Insufficient gullet depth Gullet depth unevenness
	Broken teeth		

■ Surface broach

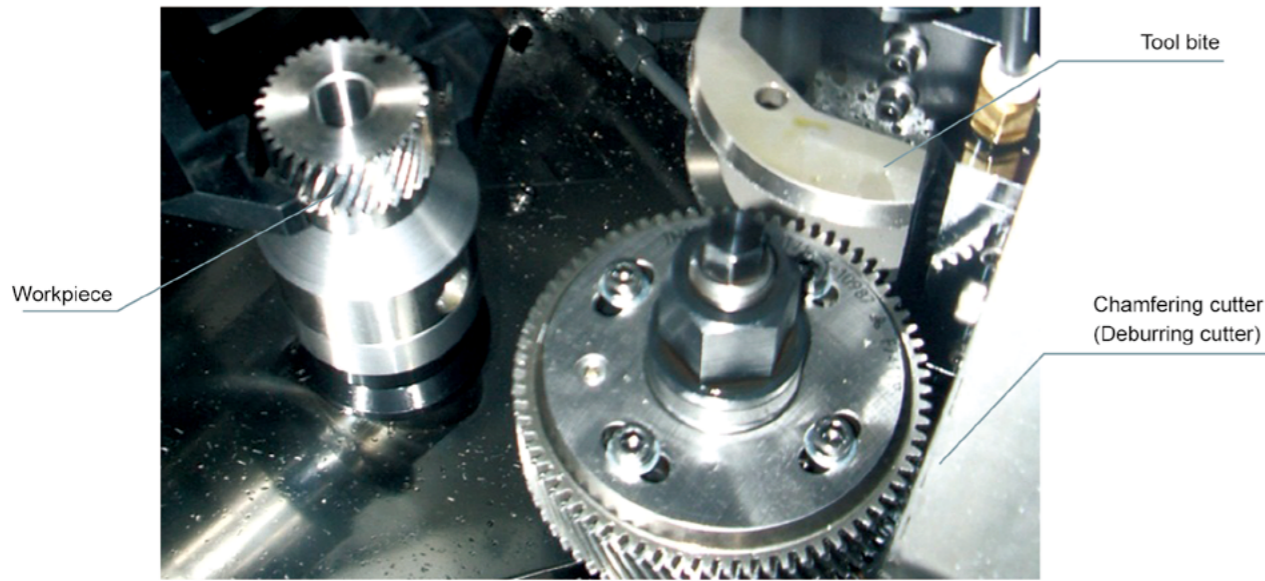
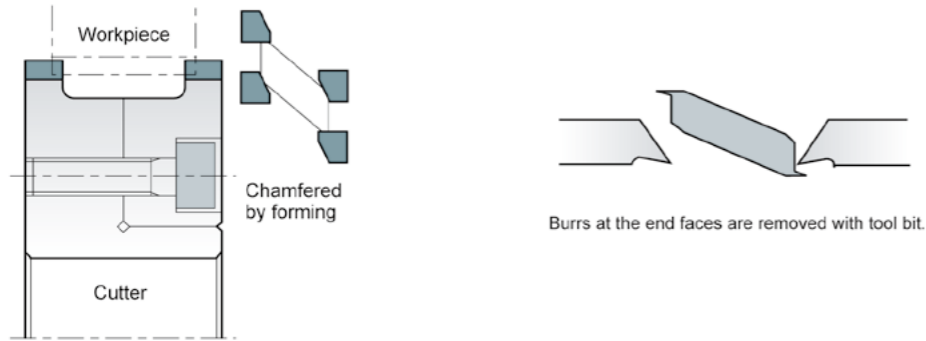
	Problem	Symptom	Cause
Workpiece	Key size	Key width error of a workpiece	1. Broach teeth width outside specifications 2. Shrinking due to poor sharpness
		Faulty workpiece key height	1. Broach height outside specifications 2. Jig size not correct
Machined surface	Flaking Scraping Edge chipping Chattering	1. Interference from parts other than teeth 7. Interference from chips 8. Improper cutting conditions 9. Improper or deteriorated cutting oil 10. Insufficient rigidity of broaching machine 11. Difficult-to-machine workpiece	
		2. Excessive cutting allowance 3. Inappropriate face angle 4. Cutting edge is worn, cracked or chipped 5. Adhesion on side of teeth 6. Shear drop	
Broach	Cracked teeth	Cracked teeth	<ul style="list-style-type: none"> Chips stuck due to faulty gullet shape Excessive land width Insufficient gullet depth Gullet depth unevenness

OTHER PRODUCTS

Chamfering Cutter (Deburring Cutter)

The chamfering cutter is used for chamfering gear edge of automobile and motorcycle reducers. After processing with hobs and shaper cutters, both edges of the gear are rolled (formed) and chamfered. Burrs that occurred in the previous processes are removed during chamfering.

Chamfering mechanism



GE15A Deburring Unit

Master Gear

The master gear is used as a master for engagement testers or for comparative measurements of tooth thickness. Our master gears can provide the high precision of the JIS M0 class.



Burnishing Cutter

The burnishing cutter is used for tapering along the teeth and lead of the spline after broaching. (This is to prevent the gear from coming off.)



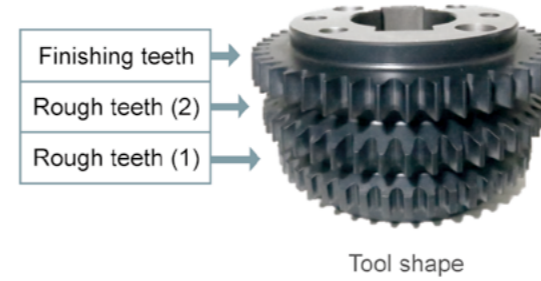
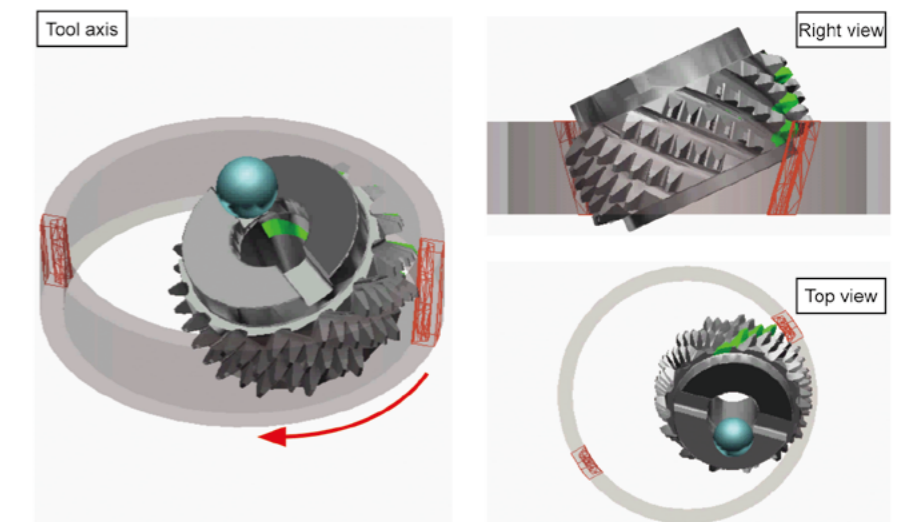
Super Skiving Cutter

The technology developed with the ZI20A internal gear grinding machine has been applied to the super skiving cutter, allowing the fastest, high-precision cutting of internal gears. It solves the issue of tool life that was a problem with previous shaper cutters, allowing stable tool life.

Skiving processing



Processing using super skiving



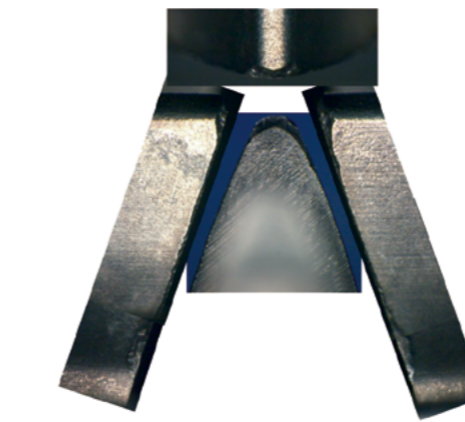
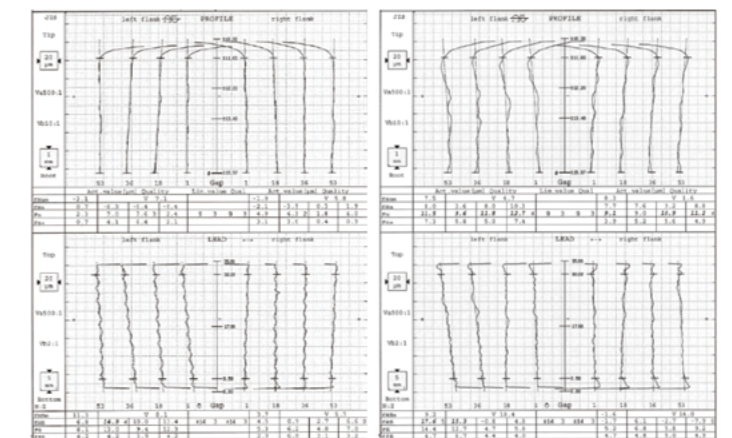
Removing the pin to disassemble it allows re-grinding in the same way as for a shaper cutter.



Example

Workpiece: Internal gear m1.5 HA20° NT70 ODφ110 Tooth length 3.65 Tooth width 40 Material SCM415 (HB180)
 Cutter: NT46 (total tooth number: 138 = 3 x 46 each of finishing teeth / rough teeth (2) / rough teeth (1)) SPUR material MX-1
 Coating: MightyShield Σ
 Cutting conditions: No. of rotations: 1,250/1,600 min-1 Ax feed 0.45/0.15mm/t.rev. C/T 60 secs. Double-cut
 Processing machine: MSS300 Super Skiving Machine

Processing precision



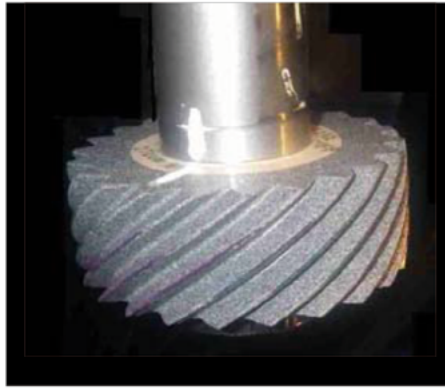
Wear status (after processing 1,200 pieces): 0.24mm

Initial processing: ISO6 class

After processing 1,200 pieces: ISO7 class

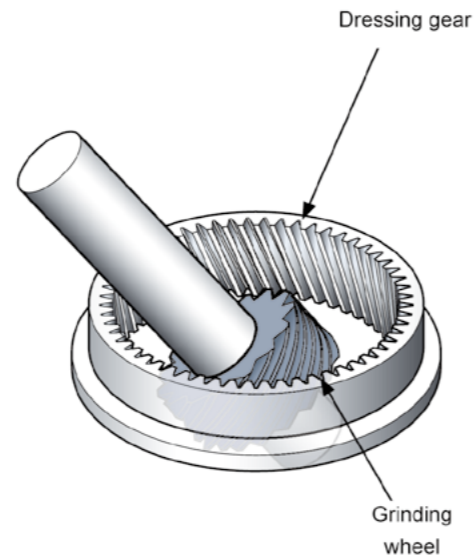
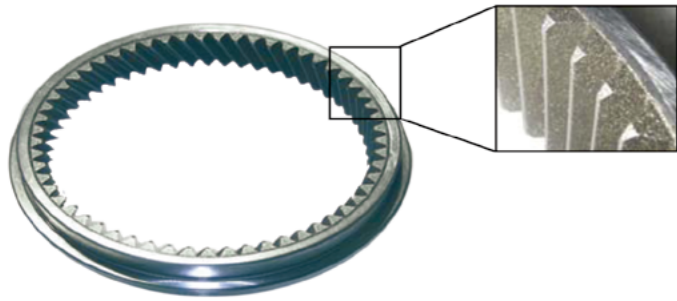
Grinding Wheel, Dressing Gear and Disc Dresser for ZI Series

■ Shaped grinding wheel

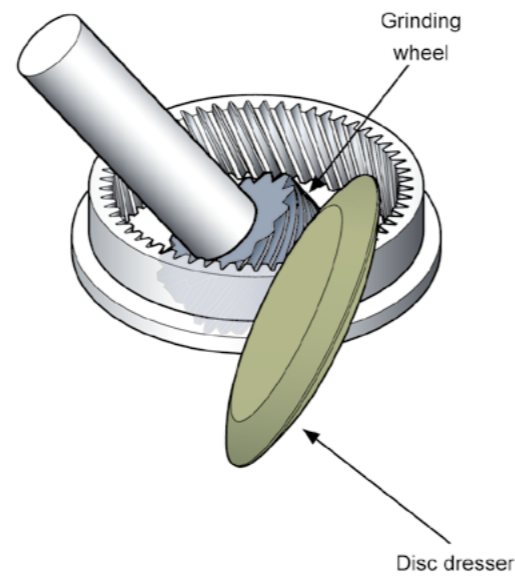


These are used for our ZI series gear grinding machines. The grinding wheel is roughly shaped, and will be reshaped to its final shape and accuracy on the grinding machine. The dressing gear is made by electrocoating diamond abrasives onto the same shaped base metal as the workpiece and engages with the grinding wheel when shaping and tothing it. The disc dresser has the same cross-sectional shape as the workpiece and moves along the teeth lead of the grinding wheel when shaping and tothing it.

■ Dressing gear



■ Disc dresser



Hirth Couplings

These are used for the high-precision angular division of cutter holders and index tables, and can go down to just 1°.

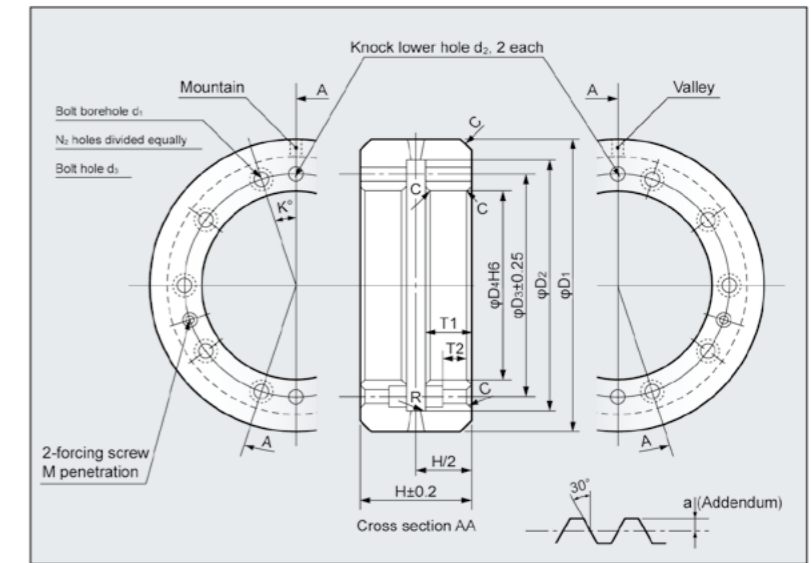
■ Double Hirth



Formula breakdown

$$320 - 225 - 72T$$

No. of teeth (N_1)
Internal diameter (D_4)
External diameter (D_1)

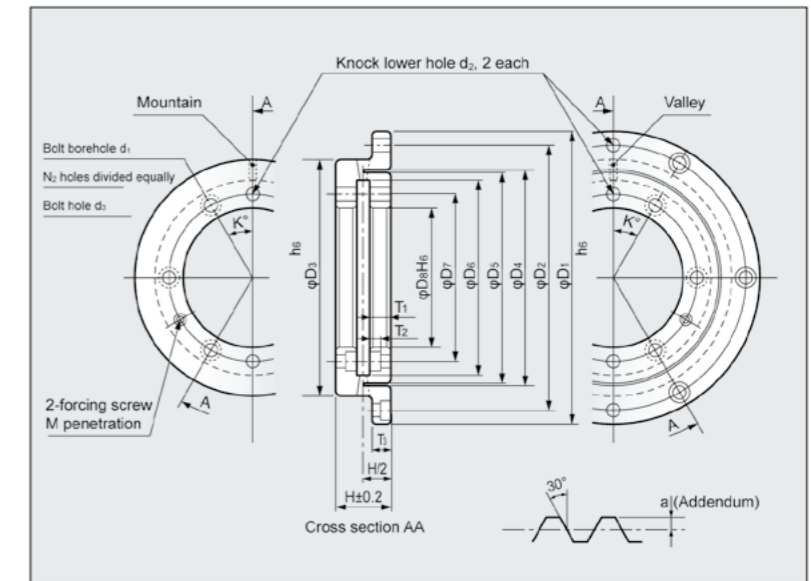


Formula breakdown

$$355 - 300 - 215 - 72T$$

No. of teeth (N_1)
Internal diameter (D_6)
External diameter (D_3)
External diameter (D_1)

■ Triple Hirth



Hobs
Shaper cutters
Shaving Cutters
Broaches
Other Products
Materials and Coatings for Tools
Estimates / Design Specifications

Hobs
Shaper cutters
Shaving Cutters
Broaches
Other Products
Materials and Coatings for Tools
Estimates / Design Specifications

Estimates / Design Specifications

Hob / Shaving Cutter Design Specifications

Customer name:		Order no.: -H		Order no.: -H	
Workpiece specifications		Chamfering		Hob processing conditions	
Part name		Amount (after gear cutting/after SV)		Cutting speed	m/min. (r.p.m)
Part no.		Diameter created (after gear cutting/after SV)		Feed	Radial mm/rev.
Module / DP		Chamfering profile		Axial	mm/rev.
Pressure angle				Processing method	Climb / Conventional
No. of teeth				No. of parts managed	
Helix angle	RH/LH, Spur			Hob shift	mm/item
Outer diameter		Profile management diameter		Hobbing machine	
Root diameter / Tooth depth		TIF diameter		SV processing conditions	
Amount of profile shift / Factor		Length of meshing normal		Processing method	Conventional / Diagonal
Tooth thickness at hobbing		Rotation angle (scope)		Underpass / Plunge	
Tooth thickness		Rotation angle (start)		No. of rotations	r.p.m
Over-pin diameter (φ)		or target workpiece specifications		Feed	mm/min. (μm/rev.)
Base tangent length T =		No. of teeth		No. of cuts	times
Tooth thickness at shaving		Outer diameter		times	T 1
Tooth thickness		Distance between centers			T 2
Over-pin diameter (φ)		Workpiece shape (has / does not have steps)		times	T 3
Base tangent length T =					B M
Shaving stock				Shaving machine	
Per tooth thickness		Tooth width		Maximum cutter diameter	
For over-pin diameter		Material / Hardness		Minimum axis distance	
For base tangent length		Accuracy		Maximum cutter width	

Hob Cutter Specifications				Shaving Cutter Specifications			
Customer tool no.		Specified / Discretionary		Customer tool no.		Semi-grand	
Outer diameter		Specified / Discretionary		Grinding method		Grand (with/without trial)	
Overall length		Specified / Discretionary		No. of teeth		Specified / Discretionary	
Bore diameter	JIS Standard	Specified / Discretionary		Nominal diameter		shape (inches)	
Bore / Edge surface key	JIS Standard	Specified / Discretionary		Bore diameter		Specified / Discretionary	
No. of starts		Specified / Discretionary		Tooth width		Specified / Discretionary	
Rake angle		None / Specified		Material	SKH51 / MACH3	Specified / Discretionary	
No. of gashes		Specified / Discretionary		Surface treatment		None / Homo treatment Super Coat / MightyShield ε	
Usage		Finishing / Pre-shaving / Pre-grinding		Cutter curve		Tool / Specified / Assumed	
Cutter tooth profile		With chamfering / With cob / topping		Cutter lead		Tool / With hollow / Specified	
Cutter accuracy	JIS A JIS AA JIS AAA Other ()			Workpiece curve		Tool / Specified separately	
Cutter material		Specified / Discretionary		Workpiece lead		Tool / Specified separately	
Coating (required / not required)		TiN / Black Dynamic / SuperDry I, II, III		Processing/measuring stance		Specified / Discretionary	
Special notes		MightyShield Σ / Other					

Shaping Cutter / Shaving Cutter Design Specifications

Customer name:		Order no.: -H		Order no.: -H	
Workpiece specifications		Chamfering		Shaping processing conditions	
Part name		Amount (after gear cutting / after SV)		No. of strokes	Strokes/minute
Part no.		Diameter created (after gear cutting/after SV)		Circumference feed	mm/rev
Module / DP		Chamfering profile		Stroke length	mm
Pressure angle				No. of cuts	
No. of teeth				No. of parts managed	
Helix angle	RH/LH, Spur			Gear shaping machine	
Outer diameter		Profile management diameter		Helical guide	
Base diameter (minor diameter) / Tooth depth		TIF diameter		SV processing conditions	
Amount of profile shift / Factor		Length of meshing normal		Processing method	Conventional / Diagonal
Tooth thickness at hobbing		Rotation angle (scope)		Underpass / Plunge	
Tooth thickness		Rotation angle (start)		No. of rotations	r.p.m
Over-pin diameter (φ)		or target workpiece specifications		Feed	mm/min. (μm/rev.)
Base tangent length T =		No. of teeth		No. of cuts	times
Tooth thickness at shaving		Outer diameter		times	T 1
Tooth thickness		Distance between centers			T 2
Over-pin diameter (φ)		Workpiece shape (has / does not have steps)		times	T 3
Base tangent length T =					B M
Shaving stock				Shaving machine	
For tooth thickness		Tooth width		Maximum cutter diameter	
For over-pin diameter		Material / Hardness		Minimum axis distance	
For base tangent length		Accuracy		Maximum cutter width	

Shaper Cutter Specifications				Shaving Cutter Specifications			
Customer tool no.		Specified / Discretionary		Customer tool no.		Semi-grand	
Outer diameter		Specified / Discretionary		Grinding method		Grand (with/without trial)	
No. of teeth		Specified / Discretionary		No. of teeth		Specified / Discretionary	
Overall length		Specified / Discretionary		Nominal diameter		shape (inches)	
Bore diameter	JIS Standard	Specified / Discretionary		Bore diameter		Specified / Discretionary	
Bore / Edge surface key	With / Without			Tooth width		Specified / Discretionary	
Cutter type		Disc / Bell / Shank		Material	SKH51 / MACH3	Specified / Discretionary	
Usage		Finishing / Pre-shaving / Pre-grinding		Surface treatment		None / Homo treatment Super Coat / MightyShield ε	
Cutter tooth profile		With chamfering / With cob / topping		Cutter curve		Tool / Specified / Assumed	
Shank shape		Specified / Discretionary		Cutter lead		Tool / With hollow / Specified	
Cutter accuracy	JIS A JIS AA Other ()			Workpiece curve		Tool / Specified separately	
Cutter material		Specified / Discretionary		Workpiece lead		Tool / Specified separately	
Coating (required / not required)		TiN / Black Dynamic / SuperDry I, II, III		Processing/measuring stance		Specified / Discretionary	
Special notes		MightyShield Σ / Other					

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Involute Spline Broach Design Specifications

Customer name: Order no.:

Note: Even if you provide a workpiece drawing or broach supply drawing, make sure it is transcribed if it is difficult to read.
 Make sure the sections are filled in. (Anything left blank will be treated as being left to our discretion.)

1	Broach supply drawing ()	No → Go to 2 Yes → Reference shank only → Go to 2 Yes → Has problems/Requires design change → Enter the details of the problem or reason for the change in 12. Yes → Design according to supply drawing → Enter any comments in 12.
2	Workpiece drawing after broach processing ()	No → Go to 3 Yes → Go to 6
3	Nominal dimensions → m, DP <input type="text"/> × PA <input type="text"/> × NT <input type="text"/>	
4	Workpiece dimensions after broach processing (include tolerances) *If chamfered, make sure <input type="text"/> is filled in. 	
5	Cutting length <input type="text"/> No. of simultaneous cuts <input type="text"/> Clamp <input type="checkbox"/>	Yes → Product Material <input type="text"/> Hardness when cut <input type="text"/> No →
6	Lower hole dimensions <input type="text"/>	Comparison with workpiece minor diameter after processing → Round teeth <input type="checkbox"/> Required (Front, Back, Both) Not required
7	Broach target dimensions → Major diameter <input type="text"/> Minor diameter <input type="text"/> BPD <input type="text"/>	
8	Front shank	Dimensions to first tooth <input type="text"/> Nominal dimensions <input type="text"/> Standard <input type="text"/> Reference drawing number <input type="text"/> Position determination <input type="checkbox"/> Required → Mountain-centered Required → Valley-centered Not required → Other → Enter the details in 12.
	Rear shank	Required → Nominal dimensions <input type="text"/> Standard <input type="text"/> Reference drawing number <input type="text"/> Not required
9	Overall length specified <input type="checkbox"/>	Yes → <input type="text"/> Tool material specified <input type="checkbox"/> No → Yes → <input type="text"/> Surface treatment specified <input type="checkbox"/> No →
10	Broaching machine model: <input type="text"/>	Maximum pulling force <input type="text"/> Stroke <input type="text"/>
11	Customer's information to be marked on cutters: <input type="text"/>	
12	Remarks (order history, customer requests, etc.) <input type="text"/>	

Key Broach Design Specifications

Customer name: Order no.:

Note: Even if you provide a workpiece drawing or broach supply drawing, make sure it is transcribed if it is difficult to read.
 Make sure the sections are filled in. (Anything left blank will be treated as being left to our discretion.)

1	Broach supply drawing ()	No → Go to 2 Yes → Reference shank only → Go to 2 Yes → Has problems/Requires design change → Enter the details of the problem or reason for the change in 10. Yes → Design according to supply drawing → Enter any comments in 10.
2	Workpiece drawing after broach processing ()	No → Go to 3 Yes → Go to 5
3	Workpiece dimensions after broach processing (include tolerances) *If chamfered, make sure <input type="text"/> is filled in. 	
4	Cutting length <input type="text"/> No. of simultaneous cuts <input type="text"/> Clamp <input type="checkbox"/>	Yes → Product Material <input type="text"/> Hardness when cut <input type="text"/> No →
5	Broach appearance shape → Finishing teeth height <input type="text"/>	Shank width <input type="text"/>
6	Front shank	Dimensions to first tooth <input type="text"/> Nominal dimensions <input type="text"/> Standard <input type="text"/> Reference drawing number <input type="text"/> Required → Nominal dimensions <input type="text"/> Standard <input type="text"/> Reference drawing number <input type="text"/> Not required
	Rear shank	Required → Nominal dimensions <input type="text"/> Standard <input type="text"/> Reference drawing number <input type="text"/> Not required
7	Overall length specified <input type="checkbox"/>	Yes → <input type="text"/> Tool material specified <input type="checkbox"/> No → Yes → <input type="text"/> Surface treatment specified <input type="checkbox"/> No →
8	Broaching machine model: <input type="text"/>	Maximum pulling force <input type="text"/> Stroke <input type="text"/>
9	Customer's information to be marked on cutters: <input type="text"/>	
10	Remarks (order history, customer requests, etc.) <input type="text"/>	

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